

Hydrogeological Investigation
4721 & 5061 Stouffville Rd
Hwy 48 & Stouffville Road Development
Whitchurch-Stouffville, Ontario

Prepared For:

Times Group Corporation

Project #: 19-043-103

Date: April 4, 2025



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April 4, 2025

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Via email: hamid@timesgroupcorp.com

RE: Hydrogeological Investigation – 4721 & 5061 Stouffville Road, Whitchurch-Stouffville, ON

DS Consultants Ltd. (DS) was retained by Times Group Corporation to conduct an additional Hydrogeological Investigation of the site located on the northeast corner of the properties located at 4721 & 5061 Stouffville Road, Whitchurch-Stouffville, ON (Site). The site is currently a part of a rural parcel used for agricultural purposes. It is understood that the proposed development will have a 19 to 29-storey high-rise buildings with three (3) levels of underground parking proposed to extend to 249.35 meters above sea level (masl) along the east side of the proposed building and two (2) levels of underground parking proposed to extend to 250.60 masl on the western side of the Building. In addition, the Site is proposed to have a permanent subfloor and perimeter foundation drainage system. It is further understood that the purpose of this Hydrogeological Investigation was to better understand the opportunities and constraints associated with the future development, and identify constraints associated with the Oak Ridges Aquifer Complex (ORAC) by drilling additional boreholes and installing monitoring wells at the target elevation of the proposed P2-P3 level permanent groundwater drainage elevation. The findings from this hydrogeological investigation were then used to estimate the construction dewatering volume and permanent drainage volume associated with the proposed P2-P3 level underground structure.

Based on the results of our investigation, the following conclusions are presented:

1. In May 2019, DS drilled one (1) borehole (BH19-5) equipped with a monitoring well within the boundary limits as part of the geotechnical, environmental, and hydrogeological investigations to a depth of 15.2 meters below ground surface (mbgs) (239.1 masl). In February 2021, DS drilled five (5) boreholes and equipped all boreholes with monitoring wells within the site boundary. The boreholes were advanced to depths ranging from 12.3 to 15.8 mbgs. Monitoring wells were screened to depths ranging from 6.0 to 15.8 mbgs.
2. In October 2024, DS drilled twelve (12) boreholes with five (5) boreholes equipped with monitoring wells within the site boundary as part of the geotechnical and hydrogeological investigations. The boreholes were advanced to depths ranging from 15.3 to 23.4 mbgs. Monitoring wells were screened to depths ranging from 7.1 to 9.1 mbgs. In February 2026, DS advanced a borehole (BH25-1) to 37.1 mbgs, to determine (if any) the extent of a deeper aquifer at the Site. A monitoring well was installed in BH25-1 to a depth of 21.3 mbgs.

3. The topography at the site ranges from approximately 254.3 to 256.7 masl generally sloping south. Willowgrove Creek is located approximately 1.5 km west of the site. Willowgrove Creek is a branch of Little Rouge Creek, which ultimately flows into Lake Ontario located approximately 25 km south of the Site. A creek is located east adjacent to the site intersecting Highway 48, and a provincially significant wetlands are located along the eastern limits of the site.
4. The overburden geology at the site generally consisted of clayey silt and silty clay overlying a sand and gravel confined aquifer.
5. As part of the hydrogeological investigation, DS completed a search of the Ministry of Environment Conservation and parks (MECP) water well records (WWRs) database. Based on the MECP WWR search, there are forty-five (45) water wells within 500 m of the site. Twenty-six (26) wells were noted as domestic (DO) wells, two (2) wells were noted for livestock (ST), one (1) well was noted for commercial (CO) use, and two (2) wells were noted as a public supply (PS) well. All other wells were noted as test holes, monitoring well, not in use or unknown. All other wells were noted as test holes, monitoring well, not in use or unknown.
6. Most communities of Stouffville continue to be served by municipal groundwater, where significant quantities of groundwater are extracted from the Oak Ridges Moraine (ORM) to service municipal water supply. A door-to-door water well survey is recommended within the study area to confirm the presence and use of identified wells.
7. Groundwater levels were measured in all available monitoring wells advanced in 2021 between January 25th and June 21st, 2021, by DS. Groundwater levels were measured in monitoring wells advanced in 2024 on November 14, 2024. The groundwater level in BH25-1 was measured on March 7th and March 24th, 2025. Groundwater levels ranged from 252.7 to 254.8 masl in monitoring wells screened in the till overburden. Sub-artesian conditions were encountered in monitoring wells screened in the underlying cohesionless deposits. Groundwater levels in monitoring wells screened in the underlying cohesionless deposits ranged from 252.8 to 256.5 masl.
8. Based on groundwater elevations, the flow direction is inferred to be southeast towards the drainage ditch, the wetland and the creek located east adjacent to the site intersecting Highway 48. DS is currently undertaking continuous groundwater level monitoring at the Site for one (1) year.
9. In total, four (4) Single Well Response Tests (slug tests) were completed by DS at the site between May 2019 and February 2021, and an additional five (5) slug tests were conducted in November 2024, and one (1) test was conducted at BH25-1 in February 2025 to estimate hydraulic conductivity (k) for the representative geological units in which the wells were screened. The k-values ranged between 3.1×10^{-7} to 4.9×10^{-6} m/s in the underlying cohesionless unit and 1.9×10^{-9} to 7.5×10^{-7} m/s in the overlying clayey silt material, indicative of medium to high permeability lithology in the lower unit and low to medium permeability in the upper unit.
10. One (1) unfiltered groundwater sample was collected from monitoring well BH19-5 and BH24-5 on October 7th, and November 15th, 2024, respectively. Samples were submitted to SGS Laboratories in Lakefield, Ontario. SGS is certified by the Canadian Association of Laboratory Accreditation Inc. (CALA)

and Canadian Standard Association (CSA). The analytical results were compared to the parameter limits listed under the York Region sanitary and storm sewer by-law 2021_102. The reported analytical results indicate manganese exceeded the York Region storm sewer criteria from BH24-5. No exceedances were reported against York Region sanitary sewer criteria and against both criteria from BH19-5.

11. The total estimated daily rate for short term construction is estimated to be approximately 54,000 L/day (54 m³/day) for P2 (east side) and 72,000 L/day (72 m³/day) for P3 (west side), with a total combined rate of 126,000 L/day (126 m³/day). This value incorporates a 100% safety factor. The estimated zone of influence (ZOI) is approximately 83 m and 71 m for P2 and P3 sides, respectively. An EASR is recommended to be submitted to the MECP for construction dewatering prior to construction.
12. An additional 340,000 Liters discharged over a 48-hour period (340 m³ over a 48-hour period) of storm water from a 25 mm precipitation even should be accounted for. Surface water and stormwater contributions during construction are no longer included in the construction groundwater taking EASR and PTTW limits as of July 1st, 2021. Stormwater contributions are to be addressed under other activity requirements.
13. Following the construction of the underground structure, long-term groundwater flow to the underfloor drainage system for the building will be a function of the upward flux and from drainage along the foundation wall. Based on the assumed design, the estimated permanent theoretical flow is approximately 22,800 L/day (22.8 m³/day) and 26,400 L/day (26.4 m³/day) for P2 and P3, respectively with a combined rate of 49,000 L/day (49 m³/day) with a 20% safety factor. Since the estimated maximum permanent drainage rate is below 50,000 L/day, a PTTW will not be required for long-term discharge. These values can change based on actual soil and groundwater conditions at the site and are to be confirmed during construction.
14. Based on results of the pre-development and post-development site water balance completed, the proposed developments will in general produce a decrease in annual evapotranspiration (11,702 m³/year), a reduction in annual infiltration (3,756 m³/year) and a general increase in annual runoff (12,763 m³/year). The effects are mainly the result of increased impervious area and decreased pervious areas of the Site. Low Impact Development (LID) measures are recommended to reduce the infiltration deficit and meet pre-development conditions.
15. The site is designated as countryside area under O.Reg 140/02: Oak Ridges Moraine Conservation Plan. Countryside Areas provide an agricultural and rural transition and buffer between the Natural Core Areas and Natural Linkage Areas and the urbanized Settlement Areas. Infrastructure uses are permitted in Countryside Areas.
16. The Site and study area are located within the Toronto Region Source Protection Area (SPA). The Site and study area are located within a Highly Vulnerable Aquifer (HVA) with a score of 6, indicating moderate risk to the aquifer from construction. However, since construction is anticipated within the

overlying till, construction is not anticipated to impact the underlying sand aquifer. The site is also located within a Significant Groundwater Recharge (SGRA). Given the low permeability of the overlying till material identified during the field investigation, the site does not readily support recharge.

17. The site and the study area are located within a municipal Wellhead Protection Area-Quantity (WHPA-Q). The site is categorized to be at moderate risk for both water taking without returning it to the same source (WHPA-Q1), and for reducing recharge to the area (WHPA-Q2). Any WHPA-Q areas where significant or moderate drinking water stress has been identified is an area where significant drinking water quantity threat activities can occur. In these areas, future activities must return water to the same source and must not reduce recharge.
18. The MECP Permit to take Water (PTTW) Open Data Catalogue was searched within a 1 km radius of the Site. The search indicated that there was (1) active PTTWs within 1 km of the site, where the source was surface water. Therefore, groundwater interferences from surrounding activities may occur.
19. The wetland falls within the zone of influence during construction dewatering. Mitigation measures should be enacted to minimize adverse effects to the creek and wetlands. A wetland water balance risk evaluation may be required for the site from the TRCA prior to development. DS recommended monitoring the water features across the site and obtaining surface water samples to establish base line water quality conditions at the site.

Should you have any questions regarding these findings, please contact the undersigned.

DS Consultants Ltd.

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Table of Contents

1.0 INTRODUCTION	1
2.0 FIELD INVESTIGATION	1
2.1 Previous Field Investigation	1
2.2 Current Field Investigation.....	2
3.0 SITE SETTING	2
3.1 Physiography and Drainage	2
3.2 Geology	2
3.2.1 Quaternary Geology	2
3.2.2 Bedrock Geology	3
3.2.3 Site Geology.....	3
4.0 HYDROGEOLOGY	4
4.1 Hydrostratigraphy	4
4.2 Local Groundwater Use	4
4.3 Groundwater Levels.....	5
4.4 Single Well Response Test Analysis	7
4.5 Groundwater Quality Analysis.....	8
5.0 CONSTRUCTION DEWATERING- UNSEALED EXCAVATION	9
5.1 Total Estimation of Flow Rate- (Short Term/Construction Dewatering).....	9
5.2 Zone of Influence During Construction	10
5.3 Permanent Drainage (Long-term Discharge).....	11
5.4 Permit Requirements	11
5.4.1 Environmental Activity and Sector Registry (EASR) /Permit to Take Water (PTTW) Application .	11
5.4.2 Discharge Permits.....	12
6.0 SITE WATER BALANCE	12
6.1 Pre-Development Water Balance.....	12
6.2 Post Development Water Balance	14
6.3 Site Water Balance Results.....	15
7.0 POTENTIAL IMPACTS.....	16
7.1 Oak Ridges Moraine Conservation Plan	16
7.2 Local Groundwater Use	16
7.3 Current PTTW Search	17
7.4 Source Protection Area	17
7.5 Highly Vulnerable Aquifer & Significant Groundwater Recharge Area (SGRA)	17
7.6 Wellhead Protection Area	17
7.7 Intake Protection Zone	18
7.8 Surface Water.....	18
8.0 LIMITATIONS	19
9.0 REFERENCES	20

FIGURES

FIGURE 1	Site Location and MECP Water Well Record Map
FIGURE 2	Surficial Geology Map
FIGURE 3	Borehole and Monitoring Well Locations
Figure 4	Groundwater Elevation Contours and Flow Direction Map
Figure 5	Geological Cross Section A-A'
Figure 6A	Pre-Development Land Use
Figure 6B	Post-Development Land Use

APPENDICES

Appendix A	Borehole Logs
Appendix B	Hydraulic Conductivity Analysis
Appendix C	Groundwater Quality Certificate of Analysis
Appendix D	MECP Water Well Records
Appendix E	Natural Heritage Map.
Appendix F	Site Water Balance

1.0 INTRODUCTION

DS Consultants Ltd. (DS) was retained by Times Group Corporation to conduct a Hydrogeological Investigation of the site located on the northeast corner of the properties located at 4721 & 5061 Stouffville Road, Whitchurch-Stouffville, ON (Site). The site is in a rural area currently used for agricultural purposes. The site is part of a larger development located at 4721 and 5061 Stouffville road, part of a rural parcel of land. DS understands that the purpose of this Hydrogeological Investigation is to better understand the opportunities and constraints associated with the future development, and identify constraints associated with the Oak Ridges Aquifer Complex (ORAC) and estimate construction dewatering volumes and permanent drainage volume associated with the underground structure.

1.2 Scope of Work

The scope of work for this investigation included:

- ◆ Site visits;
- ◆ Desktop review of pertinent geological and hydrogeological resources;
- ◆ Review the MECP Water Well Records and water use in the surrounding area;
- ◆ Field work including monitoring the well drilling program consisting of a total of nineteen (19) boreholes and twelve (12) monitoring wells;
- ◆ Conducting single well response tests (slug tests) to determine hydraulic conductivity values across the site;
- ◆ Characterize the stratigraphy and measure the ground water levels across the site;
- ◆ Estimate construction dewatering volumes and permanent drainage volumes for three (3) levels of underground parking; and
- ◆ Assess potential constraints of the site associated with future proposed development

2.0 FIELD INVESTIGATION

2.1 Previous Field Investigation

In May 2019, DS drilled one (1) borehole (BH19-5) equipped with a monitoring well within the boundary limits as part of the geotechnical, environmental, and hydrogeological investigations to a depth of 15.2 mbgs (239.1 masl). Sub-artesian conditions have been encountered at BH19-5, as water levels were found to be above the ground surface in May 2019. One (1) single well response test was completed at BH19-5 in 2019 yield a hydraulic conductivity value of 3.1×10^{-6} m/s for the screened silty sand unit.

In February 2021, DS drilled five (5) boreholes and equipped all boreholes with monitoring wells within the site boundary as part of the preliminary geotechnical and hydrogeological investigations. The boreholes were advanced to depths ranging from 12.3 to 15.8 mbgs. Monitoring wells were screened to depths ranging from 6.0 to 15.8 mbgs. All wells were completed with 50 mm diameter PVC pipes with 1.5 or 3.05 m well screens and were installed using above ground mounted protective casings. Three (3) single well response tests (SWRTs) were completed by performing a rising head test (slug test) to estimate hydraulic conductivity values of screened soils at the site.

2.2 Current Field Investigation

In October 2024, DS drilled twelve (12) boreholes with five (5) boreholes equipped with monitoring wells within the site boundary as part of the geotechnical and hydrogeological investigations. The boreholes were advanced to depths ranging from 15.3 to 23.4 mbgs. Monitoring wells were screened to depths ranging from 7.1 to 9.1 mbgs. In February 2026, DS advanced a borehole (BH25-1) to 37.1 mbgs, to determine (if any) the extent of the aquifer at the Site. A monitoring well was installed in BH25-1 to a depth of 21.3 mbgs.

All wells were completed with 50 mm diameter PVC pipes with 1.5 or 3.05 m well screens and were installed using above ground mounted protective casings. All monitoring wells were developed before any use to allow for groundwater level monitoring, hydraulic conductivity testing, and to assess groundwater quality. Six (6) single well response tests (SWRTs) were completed by performing a rising head test (slug test) to estimate hydraulic conductivity values of screened soils at the site. The borehole (BH) and monitoring well (MW) location plan is shown in **Figure 3**.

3.0 SITE SETTING

3.1 Physiography and Drainage

The site is currently being used for agricultural purposes. The topography at the site ranges from approximately 254.3 to 256.7 masl generally sloping south. Willowgrove Creek is located approximately 1.5 km west of the site. Willowgrove Creek is a branch of Little Rouge Creek, which ultimately flows into Lake Ontario located approximately 25 km south of the Site. A creek is located east adjacent to the site intersecting Highway 48, and provincially significant wetlands are located along the eastern limits of the site. The natural heritage map is shown in **Appendix E**. Drainage is generally controlled by streams and the local topography of the site.

3.2 Geology

The following presents a brief description of regional and site geology based on the review of available information and site-specific soil investigations.

3.2.1 Quaternary Geology

According to the Ontario Geological Survey mapping across the region, the site lies within the South Slope physiographic region of southern Ontario and is characterized by drumlinized till plains. The site borders the Oak Ridges Moraine (ORM) physiographic region to the north. However, according to the Ministry of

Natural Resources and Forestry, the site lies within the ORM boundary. The ORM is characterized as a linear, regionally high elevation ridge having hummocky topography that runs east to west, which is situated north of the Greater Toronto Area, and stretches approximately 160 km from the Trent River in the east to the Niagara Escarpment to the west. The ORM contains an abundant thickness of granular water bearing strata within its core that is the source for several groundwater fed tributaries that originate along the north and south slopes of the moraine. Based on a search of the MECP water well records the aquifer extends to approximately 30 mbgs within the study area. There is a possibility that the aquifer may extend beyond the approximated depth. The surficial geology at the site is characterized as clay to silt-textured till derived from glaciolacustrine deposits or shale. The overburden geology at the site generally consists of clayey silt and silty clay till overlying a sand and gravel confined aquifer. The surficial geology map is shown in **Figure 2**.

3.2.2 Bedrock Geology

According to the Ontario Geological Survey mapping across the region the bedrock at the site is predominantly comprised of shale, limestone, dolostone, siltstone of the Georgian Bay Formation; Blue Mountain Formation; Billings Formation; Collingwood Member; and Eastview Member. Bedrock was not encountered during the current investigation. Due to the thickness of the overburden and deep nature of the expected contact, it is not expected that bedrock will influence the groundwater system in respect to the current hydrogeological investigation.

3.2.3 Site Geology

On-site subsurface soils were interpreted from the boreholes/monitoring wells (BHs/MWs) drilled by DS. The locations of the BHs/MWs are shown on **Figure 3** and detailed subsurface conditions are presented on the borehole Logs in **Appendix A**. The subsurface conditions in the boreholes are summarized in the following paragraphs, and the geologic cross sections (A-A') is presented in **Figure 5**.

Topsoil/Fill: A surficial layer of topsoil of 125 to 3800 mm thick was found in all boreholes. It should be noted that the thickness of the topsoil explored at the borehole locations may not be representative of the site and should not be relied on to calculate the amount of topsoil at the site. Below the topsoil, fill materials and/or weathered/disturbed soils consisting of clayey silt to silty clay and sandy silt to silty sand were encountered in all boreholes, extending to depths varied from 0.8 to 2.4 m below ground surface. These soils were found traces of rootlets and topsoil inclusions.

Clayey Silt TO Silty Clay (Till): Cohesive deposits of clayey silt to silty clay (till) were encountered in all boreholes, extending to depths ranging from 9.0 m to 37.1 m below existing ground surface. Boreholes BH24-3 to BH24-5, BH24-9, BH24-12 and BH25-1 were terminated in the clayey silt to silty clay (till). These soils were found to be weathered/disturbed due to ploughing activities in the past. Traces of rootlets and topsoil inclusions were also observed in the weathered deposits. Occasional sand seams and cobble/boulder were present within the clayey silt to silty clay (till) deposits. These deposits were found in a firm to hard consistency.

Sandy Silt to Silty Sand Till: Sandy silt to silty sand till deposits were encountered in all boreholes, extending to depths of 12.0 to 23.4 m below existing grade. Sandy silt to silty sand till deposits were found to be in a compact to very dense state. Occasional sand seams and cobble/boulder were present within the sandy silt to silty sand till deposits.

Cohesionless Sandy Soils (Silt, Sandy Silt to Silty Sand and Sand): Cohesionless water bearing soils consisting of silt, sandy silt to silty sand and sand were encountered at various depths in all boreholes except for boreholes BH24-4 to BH24-6. The cohesionless soils were present in a compact to very dense state.

4.0 HYDROGEOLOGY

The hydrogeology at the development Site was evaluated using the on-site monitoring wells installed by DS, MECP WWRs in the study area and the Oak Ridges Moraine Groundwater Program mapping.

4.1 Hydrostratigraphy

The review of sub-surface soils and based on regional mapping from the Oak Ridges Moraine Groundwater Program mapping. Five (5) hydrostratigraphic units were identified in the vicinity of the site from youngest to oldest:

- **Oak Ridges Aquifer Complex (ORAC):** The ORAC sediments overlie a regional unconformity with infill tunnel channels forming a prominent east-west ridge. The ORAC sediments generally consist of silt and fine sands, but also include gravel seams and some clay. The aquifer is generally unconfined except for areas where it underlies the Halton Till. The ORM sediments are considered high recharge areas.
- **Lower Newmarket Till:** The Newmarket till is a thick aquitard, characterized by low hydraulic conductivity and forms an extensive sheet with various heterogeneous soil characteristics.
- **Thorncliffe Formation:** formed of poorly exposed, interbedded lake sediments and till. It generally comprises of sand and silt, clay, and till. The aquifer is confined by the Newmarket fill aquitard. The unit is characterized by sandy formations with high hydraulic conductivity.
- **Sunnybrook Drift:** Aquitard material separating the Thorncliffe deposits from the Scarborough Formation generally described as clast poor mud consisting of silt and clay.
- **Scarborough Formation:** The Scarborough formation is an aquifer formed of organic rich sands over silt and clays from melt water from glaciation which occurred about 40,000 to 90,000 years ago.

4.2 Local Groundwater Use

As part of the hydrogeological investigation, DS completed a search of the MECP water well records (WWRs) database. Based on the MECP WWR search, there are forty-five (45) water wells within 500 m of the site (**Appendix C**). Twenty-six (26) wells were noted as domestic (DO) wells, two (2) wells were noted for livestock

(ST), one (1) well was noted for commercial (CO) use, and two (2) wells were noted as a public supply (PS) well. All other wells were noted as test holes, monitoring well, not in use or unknown. **Figure 1** shows the MECP water well location plan. Most communities of Whitchurch-Stouffville continue to be served by municipal groundwater, where significant quantities of groundwater are extracted from the ORM to service municipal water supply. A door-to-door water well survey is recommended within the study area to confirm the presence and use of identified wells.

4.3 Groundwater Levels

Groundwater levels were measured in all available monitoring wells advanced in 2021 between January 25th and June 21st, 2021, by DS. Groundwater levels were measured in monitoring wells advanced in 2024 on November 14, 2024. The previously installed wells in 2021 were all found damaged during this monitoring event. The groundwater level in BH25-1 was measured on March 7th and March 24th, 2025. **Table 4-1** presents the groundwater levels in all monitoring wells. Groundwater levels ranged from 252.7 to 254.8 masl in monitoring wells screened in the till overburden (well depths ranging from 6.0 to 9.1 mbgs). Sub-artesian conditions were encountered in monitoring wells screened in the underlying cohesionless deposits (well depths ranging from 12.1 to 21.3 mbgs). Groundwater levels in monitoring wells screened in the underlying cohesionless deposits ranged from 252.8 to 256.5 masl.

Near ground surface groundwater levels, indicate that an underlying confined layer is under substantial pressure. The interpreted shallow groundwater contour map for the water level measurements is shown in **Figure 4**. Based on groundwater elevations, the flow direction is inferred to be southeast towards the drainage ditch, the wetland and the creek located east adjacent to the site intersecting Highway 48. The groundwater levels are subject to seasonal fluctuations and may vary in response to changing climate conditions and may also affect the direction of the shallow groundwater flow direction at the Site.

Table 4-1: Groundwater Levels in Monitoring Wells

Well ID	Ground Elevation (masl)	Screened Interval (mbgs)	Date	Stick-up (m)	WL (top of pip) (m)	Depth to Water (mbgs)	Groundwater Elevation (masl)
BH21-1	254.5	12.2-15.2	25-Feb-21	0.8	1.1	0.3	254.2
			13-Apr-21		2.2	1.4	253.1
			18-May-21		2.1	1.3	253.2
			21-Jun-21		2	1.3	253.2
			16-Jul-21		2.3	1.5	253
			23-Aug-21		2.4	1.6	252.9
			14-Sep-21		2.5	1.7	252.8
			13-Oct-21		2.5	1.7	252.8
			15-Nov-21		2.5	1.7	252.8
			13-Dec-21		2.5	1.7	252.8

			11-Jan-22		2.3	1.5	253.0
			15-Feb-22		2.3	1.5	253.0
			14-Mar-22		2.2	1.4	253.1
			19-Apr-22		2	1.2	253.3
BH21-2	255.2	9.1-12.1	25-Feb-21	0.9		Frozen	
			13-Apr-21		2	1.1	254.1
			18-May-21		1.3	0.4	254.8
			21-Jun-21		2.4	1.5	253.7
			16-Jul-21		1.7	0.8	254.4
			23-Aug-21		2	1.1	254.1
			14-Sep-21		2	1.1	254.1
			13-Oct-21		1.7	0.8	254.5
			15-Nov-21		1.5	0.6	254.6
			13-Dec-21		1.3	0.4	254.9
			11-Jan-22		1.3	0.3	254.9
			15-Feb-22		1.5	0.6	254.6
			14-Mar-22		1.2	0.3	254.9
			19-Apr-22		1.2	0.3	254.9
BH21-3	256.6	4.5-6.0	25-Feb-21	1	4.4	3.4	253.2
			13-Apr-21		4.1	3.1	253.5
			18-May-21		4.1	3.1	253.5
			21-Jun-21		4	3	253.6
			16-Jul-21		4.7	3.7	252.9
			23-Aug-21		4.8	3.8	252.8
			14-Sep-21		4.9	3.9	252.7
			13-Oct-21		4.9	3.9	252.7
			15-Nov-21		4.8	3.8	252.8
			13-Dec-21		4.4	3.4	253.2
			11-Jan-22		4.2	3.2	253.4
			15-Feb-22		4.5	3.5	253.1
			14-Mar-22		4.3	3.3	253.3
			19-Apr-22		3.8	2.8	253.8
BH21-4	256.7	10.7-12.2	25-Feb-21	0.9	2.6	1.7	255
			13-Apr-21		1.2	0.3	256.4
			25-Feb-21			Frozen	
			18-May-21		1.1	0.2	256.5
			21-Jun-21		1.1	0.2	256.5
			16-Jul-21		1.3	0.4	256.3
			23-Aug-21		1.3	0.4	256.3
			14-Sep-21		1.4	0.5	256.2
			13-Oct-21		1.4	0.5	256.2
			15-Nov-21		1.4	0.5	256.2
			13-Dec-21		1.4	0.5	256.2

			11-Jan-22		1.4	0.5	256.2
			15-Feb-22		1.4	0.5	256.2
			14-Mar-22		1.4	0.5	256.2
			19-Apr-22		1.4	0.5	256.2
			13-Apr-21		2.9	2	253.6
			18-May-21		1	0.1	255.5
			21-Jun-21		2.1	1.2	254.4
			23-Aug-21		1.8	0.9	254.7
			14-Sep-21		1.6	0.7	254.9
			13-Oct-21		1.2	0.4	255.3
			15-Nov-21		1.1	0.3	255.3
			13-Dec-21		0.8	0	255.6
			11-Jan-22		0.9	0.1	255.5
			15-Feb-22		1.1	0.3	255.3
			14-Mar-22		0.8	-0.1	255.7
			19-Apr-22		0.7	-0.2	255.8
			13-Apr-21		0.8	0	254.3
			18-May-21		0.9	0.1	254.2
			21-Jun-21		1	0.2	254.1
			16-Jul-21		1.3	0.5	253.8
			23-Aug-21		-	Not accessible	Not accessible
			14-Sep-21		1.5	0.7	253.6
			13-Oct-21		1.2	0.4	253.9
			15-Nov-21		1	0.3	254.0
			13-Dec-21		0.8	0	254.3
			11-Jan-22		0.7	-0.1	254.4
			15-Feb-22		0.7	-0.1	254.4
			14-Mar-22		0.7	-0.1	254.4
			19-Apr-22		0.7	-0.1	254.4
			07-Oct-24		1.2	0.4	253.9
BH24-1	256.6	6.1-9.1	13-Nov-24	0.9	2.7	1.8	254.8
BH24-4	255.4	4.6-7.6	13-Nov-24	0.9	2.2	1.3	254.1
BH24-5	254.9	4.6-7.7	13-Nov-24	0.9	2.3	1.4	253.5
BH24-8	254.5	4.1-7.1	13-Nov-24	0.9	2.3	1.4	253.1
BH24-9	255.8	5.6-8.6	13-Nov-24	0.9	3.1	2.2	253.6
			07-Mar-25		1.09	0.2	254.1
BH25-1	254.3	16.3-21.3	24-Mar-25	0.94	0.78	-0.2	254.5

4.4 Single Well Response Test Analysis

In total, four (4) Single Well Response Tests (slug tests) were completed by DS at the site between May 2019 and February 2021. An additional five (5) slug tests were conducted in November 2024, and one (1) test was conducted at BH25-1 in February 2025 to estimate hydraulic conductivity (k) for the representative

geological units in which the wells were screened. The testing was completed using data loggers placed at the bottom of the monitoring wells to accurately measure the change in the hydraulic head versus time. Hydraulic conductivity (k) values were calculated using the Bouwer and Rice method using the AquiferTest® Software. The semi-log plots for normalized drawdown versus time are provided in **Appendix B**. The k-values ranged between 3.1×10^{-7} to 4.9×10^{-6} m/s in the underlying cohesionless unit and 1.9×10^{-9} to 7.5×10^{-7} m/s in the overlying clayey silt material, indicative of medium to high permeability lithology in the lower unit and low to medium permeability in the upper unit. **Table 4-2** presents the Hydraulic Conductivity (k) values for the representative geological units.

Table 4-2: Summary of Hydraulic Conductivity (k) Test Results

Well ID	Screened Interval (mbgs)	Screened Formation	K-value (m/s)
BH21-1	12.2-15.2	Sand and Gravel, Silty Sand Till	1.6×10^{-6}
BH21-3	4.5-6.0	Sand	4.9×10^{-6}
BH21-4	10.7-12.2	Sandy Silt Till	6.8×10^{-7}
BH19-5	12.2-15.2	Silty Sand to Sandy Silt, Sand and Gravel	3.1×10^{-7}
BH25-1	16.3-21.3	Silty Sand and Silty Sand to Sandy Silt Till	3.2×10^{-7}
Geomean			8.8×10^{-7}
BH24-1	6.1-9.1	Silty Clay Till & Clayey Silt	1.1×10^{-8}
BH24-4	4.6-7.6	Clayey Silt to Silty Clay Till	7.5×10^{-7}
BH24-5	4.6-7.6	Clayey Silt	7.1×10^{-8}
BH24-8	4.1-7.1	Clayey Silt Till & Clayey Silt	7.5×10^{-8}
BH24-9	5.6-8.6	Clayey Silt	1.9×10^{-9}
Geomean			3.8×10^{-8}

4.5 Groundwater Quality Analysis

To assess the suitability for discharge of groundwater to the York Region sewers, one (1) unfiltered groundwater sample was collected from monitoring wells BH19-5 and BH24-5 on October 7th and November 15th, 2024, respectively. The samples were placed in pre-cleaned laboratory supplied vials and/or bottles provided with analytical test group-specific preservatives, as required. Dedicated nitrile gloves were used during sample handling. The groundwater samples were submitted to SGS Laboratories in Lakefield, Ontario. SGS is certified by the Canadian Association of Laboratory Accreditation Inc. (CALA) and the Canadian Standard Association (CSA). The analytical results were compared to the parameter limits listed under the York Region Sewer Use Bylaw 2021_102. The reported analytical results indicate manganese exceeded the York Region storm sewer criteria from BH24-5. No exceedances were reported against York

Region sanitary sewer criteria from both samples. **Table 4-3** presents a summary of the exceeded parameters, and the certificate of analysis is provided in **Appendix C**.

Table 4-3: Parameters in Groundwater Exceeding the York Region Sewer Use Bylaw

Parameter	Unit	York Region Storm Sewer By-Law Criteria	York Region Sanitary Sewer By-Law Criteria	BH19-5	BH24-5
Manganese	mg/L	0.15	5	0.0131	0.323
Note: 0.00 - Exceeded Storm Bylaw 0.00 - Exceeded Sanitary Bylaw					

5.0 CONSTRUCTION DEWATERING- UNSEALED EXCAVATION

Construction dewatering is anticipated within the site boundaries for the proposed development. Construction dewatering estimates were based on the site area indicated on site plan designs. The current proposed development is to consist of a 19 to 29-storey high-rise building with P3 extending to 249.35 masl along the east side of the proposed building P2 extending to 250.60 masl on the western side of the Building. Footings are estimated to extend 2.5m below the P2 floor slab (248.10 masl) and P3 floor slab (246.85 masl). The groundwater level should be lowered 1 m below the footings of P2 and P3 to 247.10 masl and 245.85 mas, respectively. Dewatering will be required for the excavation below the groundwater table, and depressurization of the aquifer will be required for any excavations below the estimated safe excavation depths (SEDs). SEDs are discussed in the geotechnical report under a separate cover. The following section calculates the estimated dewatering required during the construction of the proposed developments using the steady-state flow equation for an unsealed excavation.

5.1 Total Estimation of Flow Rate- (Short Term/Construction Dewatering)

This section calculates the estimated dewatering needed considering the open-cut excavation methods using the Dupuit expression for an unconfined aquifer in steady-state conditions.

$$Q = \frac{\pi K (H^2 - h^2)}{2.3 \log\left(\frac{R_0}{r_e}\right)} \quad \text{Equation 4.1}$$

$$R_0 = C(H - h)\sqrt{k} \quad \text{Equation 4.2}$$

$$r_e = \sqrt{\frac{ab}{\pi}} \quad \text{Equation 4.3}$$

Where,

	P2 (West)	P3 (East)
H- Initial Elevation of Water Table (m)	8.4	11
h-Final Elevation of Water Table (m)	1	1
K- Hydraulic Conductivity (m/s)	1.6×10^{-7} (geomean for area)	2.9×10^{-7} (geomean for area)
Ro- Radius of Influence (m)	83	71
Re- Equivalent Radius (m)	74	54.7
A- Area (m ²)	17,300	9,400
C- Dimensionless Constant	3	3
Q- Flow Rate (L/day)	27,000	36,000
Q- Maximum Flow Rate (m³/day) 100% safety factor	54,000	72,000

The total estimated daily rate for short term construction is estimated to be approximately **54,000 L/day (54 m³/day)** for P2 (east side) and **72,000 L/day (72 m³/day)** for P3 (west side), with a total combined rate of **126,000 L/day (126 m³/day)**. This value incorporates a 100% safety factor. It is expected that the initial dewatering rate will be higher to remove groundwater from within the overburden formation. The dewatering rates are expected to decrease once the target water level is achieved in the excavation footprint as groundwater will have been removed locally from storage resulting in lower seepage rates into the excavation. The maximum flow calculation is intended to provide conservative value to account for unforeseeable conditions that may arise during construction.

Surface water runoff and precipitation may accumulate in the excavation resulting in additional water discharge. Water discharge will depend on the size of the excavation, precipitation intensity and excavation method. To represent a 'significant' precipitation event, an estimated 25 mm precipitation event in 24 hours was used to estimate potential storm water discharge. This would account for approximately **340,000 L discharged over a 48-hour period (340 m³ over a 48-hour period)** for the entire Site. Surface water and stormwater contributions during construction are no longer included in the construction groundwater taking EASR and PTTW limits as of July 1st, 2021. Stormwater contributions are to be addressed under other activity requirements.

5.2 Zone of Influence During Construction

The radius of influence (Ro) for the construction dewatering was calculated based on the Sichardt equation (Equation 4.2). Ro is the distance at which the drawdown resulting from pumping is negligible. The equation is empirical and was developed to provide representative flow rates using the steady-state flow dewatering equations as indicated above. Under steady-state conditions, Ro of pumping will extend until boundary flow conditions are reached and sufficient water inputs are equal to the discharge rate due to pumping. Therefore, the Sichardt equation is used to provide a representative flow rate but is not precise in determining the actual radius of influence by pumping. Based on Sichardt equation the zone of influence for the proposed development at the site is approximately 83 m and 71 m for P2 and P3 sides, respectively.

5.3 Permanent Drainage (Long-term Discharge)

A subfloor and perimeter drainage system (PDS) will be required to be implemented to manage groundwater long-term. Continuous groundwater collection and discharge to the Region's sewer will be required. Alternatively, the underground parking structures may be designed as water-tight structures, and groundwater discharge will not be required. Following the construction of the underground structure, long-term groundwater flow to the underfloor drainage system for the building will be a function of the upward flux and drainage along the foundation wall. To estimate the groundwater flow to the future sub-, drain the Dupuit equation was used to obtain a flow rate.

	P2 (West)	P3 (East)
H- Initial Elevation of Water Table (m)	6.4	7.0
h-Final Elevation of Water Table (m)	0.5	0.5
K- Hydraulic Conductivity (m/s)	1.6×10^{-7} (geomean for area)	2.9×10^{-7} (geomean for area)
Ro- Radius of Influence (m)	81	65
Re- Equivalent Radius (m)	74.2	54.7
A- Area (m ²)	17,300	9,400
C- Dimensionless Constant	3	3
Q- Flow Rate (m³/day)	19,000	22,000
Q- Maximum Flow Rate (m³/day) 20% safety factor	22,800	26,400

Based on the assumed design, the estimated permanent theoretical flow is approximately **22,800 L/day (22.8 m³/day)** and **26,400 L/day (26.8 m³/day)** for P2 and P3, respectively with a combined rate of **49,000 L/day (49 m³/day)** with a 20% safety factor. The drainage control system around and beneath the buildings should be designed with enough capacity to handle the expected permanent volume. This value is recommended to be verified once the underground construction is completed, and access is provided to DS to assess actual flow rates at the sumps.

5.4 Permit Requirements

5.4.1 Environmental Activity and Sector Registry (EASR) /Permit to Take Water (PTTW) Application

An EASR is required to be submitted to the MECP if the taking of groundwater and stormwater for a temporary construction project is between 50,000 L/day and 400,000 L/ day. The EASR application is an online registry and should be submitted to the MECP before any construction dewatering. A PTTW is only required to be submitted to the MECP if the taking of groundwater and stormwater for a temporary construction project is more than 400,000 L/ day.

Since the expected design dewatering rates for the unsealed excavation is above 50,000 L/day, an EASR application is required for short-term dewatering during construction.

Since the estimated maximum permanent drainage rate is below 50,000 L/day, a PTTW will not be required for long-term discharge. These values can change based on actual soil and groundwater conditions at the site and will be confirmed during construction.

5.4.2 Discharge Permits

A discharge permit may be required from the York Region if private water is to be sent to the storm sewer system for construction dewatering and permanent drainage.

6.0 SITE WATER BALANCE

To understand and compare existing hydrologic conditions, a Thornthwaite site water balance was completed. The Thornthwaite water balance (Thornthwaite, 1948; Mather, 1978; 1979) is an accounting type method used to analyze the allocation of water among various components of the hydrologic cycle. Inputs to the model are monthly temperature, Site latitude, precipitation, and stormwater run-off. Outputs include monthly potential and actual evapotranspiration, evaporation, water surplus, total infiltration, and total runoff. For ease of calculation, a spreadsheet model was used for the computation.

When precipitation (P) occurs, it can either runoff (R) through the surface water system, infiltrate (I) to the water table, or evaporate/evapotranspiration (ET) from the earth's surface and vegetation. The sum of R and I is termed as the water surplus (S). When long-term averages of P, R, I and ET are used, there is no net change in groundwater storage (ST). Annually, however, there is a potential for small changes in ST. The annual water budget can be stated as $P = ET + R + I + ST$ and the components are discussed below.

6.1 Pre-Development Water Balance

The Site has a total approximate area of 26,748 m² and is predominantly comprised of agricultural land. **Figure 6A** shows the pre-development conceptual model considered for establishing current hydrologic conditions. To predict outputs of the pre-development water balance, various inputs were entered into the Thornthwaite model including monthly precipitation and temperature, site latitude, water holding capacity values for native soils and factors of infiltration. Various inputs and outputs of the model are summarized below.

The average annual precipitation rate for the area is approximately 895 mm/year. In the pervious area of the Site, the PET is estimated to be 612 mm/year, which is approximately 68% of the total annual precipitation rate.

Precipitation (P)

Based on the 30-year average for the Richmond Hill Climate Station in Ontario, the average precipitation for the area is about 895 mm/year for the period between 1981 and 2010. Also, the average monthly temperature from this station has been used. The monthly distribution of precipitation is presented in **Table 1, Appendix F**.

Storage (St)

Groundwater storage (ST) of native soils for the existing Site was estimated using values of Water Holding Capacity (mm) of respective land use and soil types identified in Table 3.1 of the Storm Water Management (SWM) Planning & Design Manual (MOE, March 2003). The land uses, soil types and respective water

holding capacities chosen to represent existing conditions at the Site include the following with their respective water holding capacity applied to March for monthly calculations:

- Agricultural/Moderately Rooted Crops, Silt Soils– 200 mm

Using the procedures outlined in the SWM Planning & Design Manual for the above land use and soil type, the annual change in storage is zero (0).

Evapotranspiration (Et)

Monthly Potential Evapotranspiration (PET) is estimated using monthly temperature data and is defined as a water loss from a homogeneous vegetation-covered area that never lacks water (Thornthwaite, 1948; Mather, 1978). In the Thornthwaite water balance model, PET is calculated using the Hamon equation (Hamon, 1961);

$$PET_{Hamon} = 13.97 * d * D^2 * W_t$$

Where:

d = the number of days in the month

D = the mean monthly hours of daylight in units of 12 hours

W_t = a saturated water vapour density term = $4.95 * e^{0.627/T}$

T = the monthly mean temperature in degrees Celsius

The calculated Actual Evapotranspiration (AET) is based on PET and changes in ST (ΔST). Where there is not enough P to satisfy PET, a reduction in ST occurs. As a result, volumes of AET are less than PET. Also, it is assumed that evaporation will occur and will amount to approximately 15% of the total precipitation for an impervious cover.

Precipitation Surplus (S)

Precipitation surplus is calculated as P–ET. For pervious areas, ET is considered AET and for impervious areas, ET is evaporation.

Infiltration (I) and Runoff (R)

For pervious areas, precipitation surplus has two (2) components in the Thornthwaite model: a runoff component (overland flow that occurs when soil moisture capacity is exceeded) and an infiltration component. The accumulation of infiltration factors for topography, soil types and cover as prescribed in Table 3.1 of the SWM Planning & Design Manual give infiltration factors for existing conditions on the Site as shown below in **Table 6-1**. The runoff component calculated in the pre-development model is the remaining volume of precipitation surplus following AET, ET, and infiltration.

Based on the above, the resulting annual evapotranspiration, infiltration and runoff volumes for each area of the Site during the pre-development period is summarized in **Table 6-1 below**.

Table 6-1 - Existing Conditions – Infiltration Factor

Land uses / soil types	Topography	Soil	Cover	Total Infiltration Factor
Agricultural/Moderately Rooted Crop	0.3	0.2	0.1	0.6

Table 6-2 – Summary of Pre-Development Water Balance

Land Uses / Soil Types	ET Volume (m ³ /year)	AET Volume (m ³ /year)	Infiltration Volume (m ³ /year)	Runoff Volume (m ³ /year)
Agricultural/Moderately Rooted Crop	NIL	15,409	5,122	3,414

The detailed calculations are provided in **Table 2, Appendix E**

6.2 Post Development Water Balance

Post-development conditions include impervious areas and pervious areas of park area (urban lawn), with silt loam soils. To predict outputs of the post-development water balance, the same 30-year average climate data and site latitude inputs were used. Changes in land use including landscaped areas include a reduction in soil water holding capacity inputs and factors of infiltration. **Figure 6B** shows the post-development conceptual model considered for establishing current hydrologic conditions. Various inputs and outputs of the post-development model are presented in **Table 3, Appendix F**.

PRECIPITATION (P)

Based on the 30-year average for the Richmond Hill WWTP Climate Station, the average precipitation for the area is about 895 mm/year for the period between 1981 and 2010. Also, the average monthly temperature from this station has been used. The monthly distribution of precipitation is presented in **Table 1, Appendix F**.

Storage (St)

The land uses, soil types and respective water holding capacities chosen to represent existing conditions at the Site including the following with their respective water holding capacity applied to March for monthly calculations:

- Park (Urban Lawns)/Silt Loam – 125 mm

Like the pre-development conditions, using the procedures outlined in the SWM Planning & Design Manual for each land use, the annual change in storage is 0. The monthly distribution of ST for each of the land use/soil types is presented in **Table 3, Appendix F**.

Evapotranspiration (Et)

The proposed plans for development during the post-construction period will result in an increase in the total impervious hard surfaces across the Site. The total area of impervious surfaces following the proposed plans for construction is approximately 20,063 m². In the impervious areas, it is assumed that only evaporation will occur and will amount to approximately 15% of the total precipitation. Considering a total annual precipitation of 895 mm/year, evaporation is estimated at 122 mm/year. On this basis, the total annual volume of evaporation is estimated at 134 m³/year. The detailed calculations for evaporation are included in **Table 3, Appendix F**.

For post-development pervious areas, monthly PET is estimated using the same inputs and calculations described in the pre-development model respective of land use and soil moisture holding capacity. In the post-development scenario, annual AET is 3,707 m³/year for the pervious landscaped/developmental area of the Site. The monthly distribution of post-development AET and detailed calculations are presented in **Table 3, Appendix F**.

Precipitation Surplus (S)

For post-development pervious surfaces at the Site, precipitation surplus is calculated as the difference between precipitation and actual evapotranspiration (P–AET), which is estimated to be 358 mm/year for pervious landscaped areas.

For Impervious surfaces at the Site, surplus is P–ET where ET is estimated at 15% of P. The resulting precipitation surplus is about 134 mm/yr. The more detailed calculations are included in **Table 3, Appendix F**.

Infiltration (I) and Runoff (R)

The accumulation of infiltration factors for topography, soil types and cover are prescribed in Table 3.1 of the SWM Planning & Design Manual. The annual volume of post-development infiltration for the development is estimated at 1,366 m³/year.

The runoff component calculated in the post-development model is the remaining volume of precipitation surplus following infiltration. Considering the precipitation surpluses and the total infiltration volume, the total runoff for the development is approximately 16,177 m³/year. Detailed calculations and the monthly distribution of infiltration and runoff are presented in **Table 3, Appendix F**.

6.3 Site Water Balance Results

Based on results of the pre-development and post-development water balance completed, the proposed developments will in general produce a decrease in annual evapotranspiration over the Site, a reduction in annual infiltration and a general increase in annual runoff at the Site. The effects are mainly the result of increased impervious area and decreased pervious areas of the Site. The proposed development will produce an infiltration deficit of 3,756 m³/year and an increase in annual runoff of 12,763 m³/year.

Table 6-3 below summarizes the pre- and post-development conditions with and without mitigation measures. LID measures are recommended to reduce the infiltration deficit and meet pre-development conditions. In-situ infiltration tests will be conducted once LID inverts are provided to DS for review. A minimum 1 m clearance must be maintained between the bottom invert of LID measures and the groundwater table. A mitigated water balance will be provided once LID design is provided to DS for review.

Table 6-3- Summary of Water Balance Analysis – Pre-Development and Post-Development

Hydrologic Output	Pre-Development	Post-Development	Change (Pre- to Post Development)
Proposed Development Area (m ²)	26,748	26,748	0
Precipitation (m ³ /year)	23,945	23,945	0
Total Evaporation (m ³ /year)	0	2,694	2,694
Total AET (m ³ /year)	15,409	3,707	-11,702
Total Infiltration (m ³ /year)	5,122	1,366	-3,756
Total Runoff (m ³ /year)	3,414	16,177	12,763

7.0 POTENTIAL IMPACTS

The potential impacts associated with a development occurring at the site are presented in the sections below.

7.1 Oak Ridges Moraine Conservation Plan

The Site falls under O.Reg 140/02: Oak Ridges Moraine Conservation Plan. The ORM Conservation Plan is an ecologically based plan that provides land use and resource management direction for land and water within the Moraine. The site is categorized is designated as countryside area.

Countryside Areas provide an agricultural and rural transition and buffer between the Natural Core Areas and Natural Linkage Areas and the urbanized Settlement Areas. Infrastructure uses are permitted in Countryside Areas. Residential developments, and small-scale commercial, industrial, and institutional uses are permitted in Countryside Areas. Additional permitted land uses are outlined in section 12(3) and section 13(3) of O.Reg 140/02. The Ontario Ministry of Natural Resources and Forestry Map is shown in **Appendix E**.

7.2 Local Groundwater Use

The MECP water well record search identified multiple water supply wells within the study area. Prior to any development, it is recommended that a door-to-door water well survey be conducted within the study area to confirm the presence and the use of the water supply wells identified in the MEC WWRs, and to assess potential short-term and long-term impacts to private water wells that may occur from dewatering activities at the site.

7.3 Current PTTW Search

The MECP Permit to take Water (PTTW) Open Data Catalogue was searched within a 1 km radius of the Site. The search indicated that there is one (1) active PTTWs within 1 km of the Site where the source was surface water. Therefore, groundwater interferences from surrounding activities may occur. The PTTW search is summarized in **Table 7-1** below.

Table 7-1: PTTW Search within 1 km of Site

Permit Number	Permit Holder Name	Purpose	Specific Purpose	Max Litres Per Day	Source Type	Distance from Site (km)
2307-ALLT4C	63 Golf Inc. operating as Spring Lakes Golf Club	Commercial	Golf Course Irrigation	3,410,000	Surface Water	0.99

7.4 Source Protection Area

The site is located within the Toronto Region Source Protection Area (SPA). The site was identified to be within an area of significant groundwater recharge with a designated score of 6. Significant groundwater recharge areas are characterized by porous soils such as sand and gravel, which allow water to seep easily to the ground. A recharge area is considered significant when it helps maintain water levels in an aquifer that supplies a community with drinking water. Groundwater impacts as a result of construction should be assessed and minimize potential impacts to drinking water.

7.5 Highly Vulnerable Aquifer & Significant Groundwater Recharge Area (SGRA)

The site is located within a Highly Vulnerable Aquifer (HVA) with a score of 6, indicating a moderate risk to the aquifer from construction activities. However, since construction is anticipated within the overlying till, construction is not anticipated to impact the underlying sand aquifer. HVAs are aquifers that are more susceptible to contamination generally consisting of granular material (i.e., sand & gravel, and fractured rock near the surface). The Site is also located within a Significant Groundwater Recharge Area (SGRA) where storm water can easily seep into the ground and replenish the aquifer. SGRAs help maintain the water level in the aquifers that supply drinking water in the area. Given the low permeability of the overlying till material identified during the field investigation, the site does not readily support recharge.

7.6 Wellhead Protection Area

The site and the study area are located within a municipal Wellhead Protection Area-Quantity (WHPA-Q). The site is categorized to be at moderate risk for both water taking without returning it to the same source (WHPA-Q1), and for reducing recharge to the area (WHPA-Q2). Any WHPA-Q areas where significant or moderate drinking water stress has been identified is an area where significant drinking water quantity

threat activities can occur. In these areas, future activities must return water to the same source and must not reduce recharge. Areas where a PTTW is required under a moderate risk WHPA-Q must demonstrate that the water taking can be maintained on a sustainable basis; will not affect the ability of the aquifer to meet the municipal water supply requirements for the current and planned service capacity; and will ensure the hydrological integrity of municipal wells will be maintained.

7.7 Intake Protection Zone

The site and the study area are not located within a water intake protection zone (IPZ). No IPZ impacts are anticipated due to the proposed temporary dewatering.

7.8 Surface Water

A creek intersects highway 48 located east of the site and provincially significant wetlands are located along the eastern limits of the site. The wetland falls within the zone of influence during construction dewatering. Mitigation measures should be enacted to minimize adverse effects to the creek and wetlands. A wetland water balance risk evaluation may be required for the site from the TRCA prior to development. DS recommended monitoring the water features across the site and obtaining surface water samples to establish base line water quality conditions at the site.

8.0 LIMITATIONS

This report was prepared for the sole use of Life Construction Inc. the addressee to provide an assessment of the hydrogeological conditions on the property. The information presented in this report is based on information collected during the completion of the hydrogeological investigation by DS Consultants Ltd. DS Consultants Ltd. was required to use and rely upon various information sources produced by other parties. The information provided in this report reflects DS' judgment in light of the information available at the time of report preparation. This report may not be relied upon by any other person or entity without the written authorization of DS Consultants Ltd. The scope of services performed in the execution of this investigation may not be appropriate to satisfy the needs of other users, and any use or reuse of this documents or findings, conclusions and recommendations represented herein, is at the sole risk of said users. The conclusions drawn from the Hydrogeological report were based on information at selected observation and sampling locations. Different conditions between and beyond these locations may become apparent during future investigations or on-site work, which could not be detected or anticipated at the time of this investigation. DS Consultants Ltd. cannot be held responsible for hydrogeological conditions at the site that was not apparent from the available information.

Should you have any questions regarding these findings, please do not hesitate to contact the undersigned.

DS Consultants Ltd.

Prepared By:



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Project Manager

Reviewed By:



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Senior Project Manager (Hydrogeology)

9.0 REFERENCES

Approved Source Protection Plan: CTS Source Protection Region. Prepared by CTC Source Protection Region, July 2015.

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Freeze, R.A. and J.A. Cherry. "Groundwater". Prentice-Hall, Inc. Englewood Cliffs, NJ. 1979.

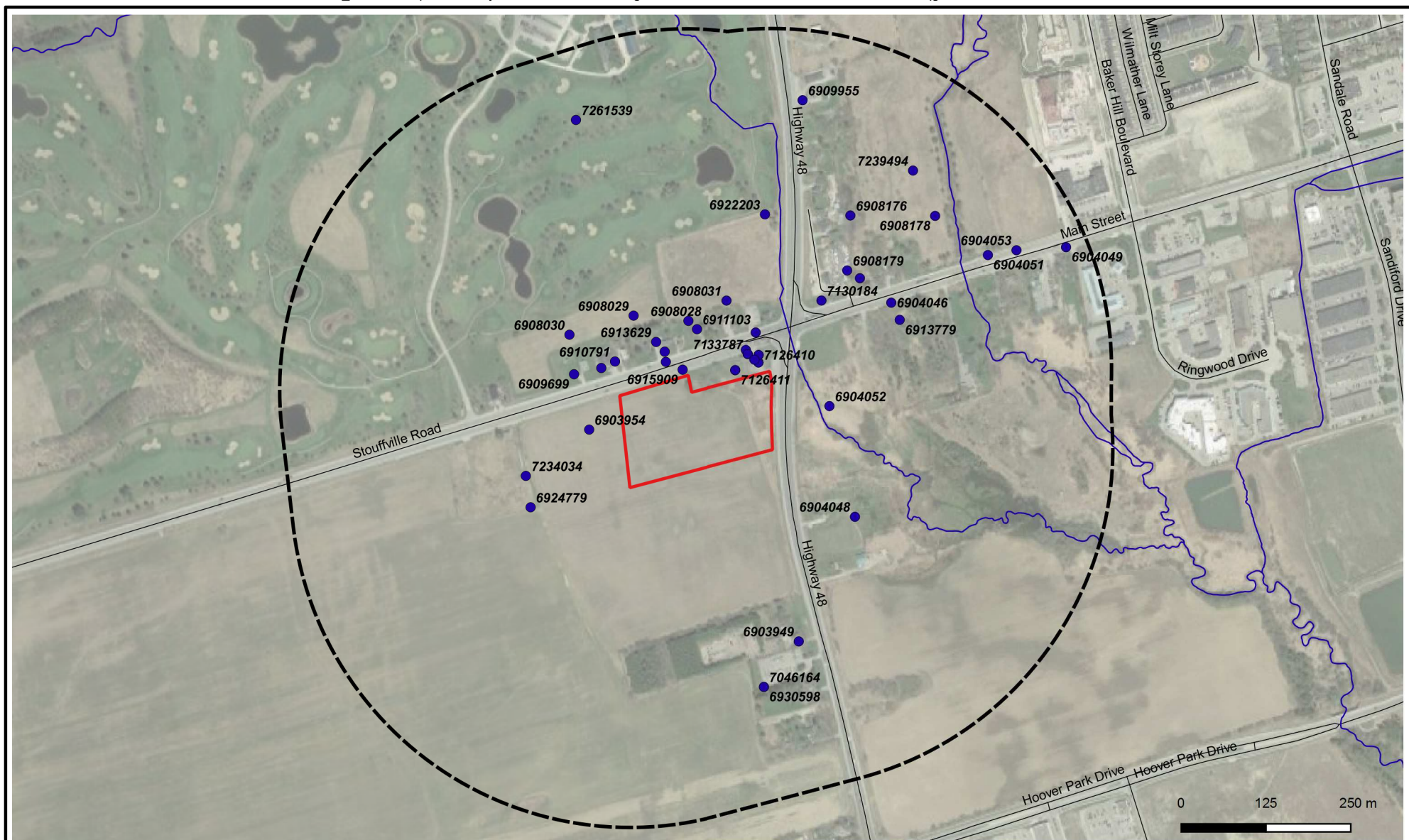
Ontario Regulation 140/02- Oak Ridges Moraine Conservation Act- 2001

Ontario Regulation 153/04 made under the Environmental Protection Act, July 1, 2011.

Ontario Regulation 245/11- Environmental Activity and Sector Registry.



Figures



Legend

- Approx Property Boundary
- 500m Buffer
- Registered Water Well (MECP WWR)



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Client:

TIMES GROUP

Project:

HYDROGEOLOGICAL INVESTIGATION
5061-4721 Stouffville Road, Whitchurch-Stouffville, ON

Title:

SITE LOCATION AND MECP WELL RECORDS

Size:
8.5 x 11

Approved By: **D.G**

Drawn By: **S.Y**

Date: **June 2021**

Rev:
0

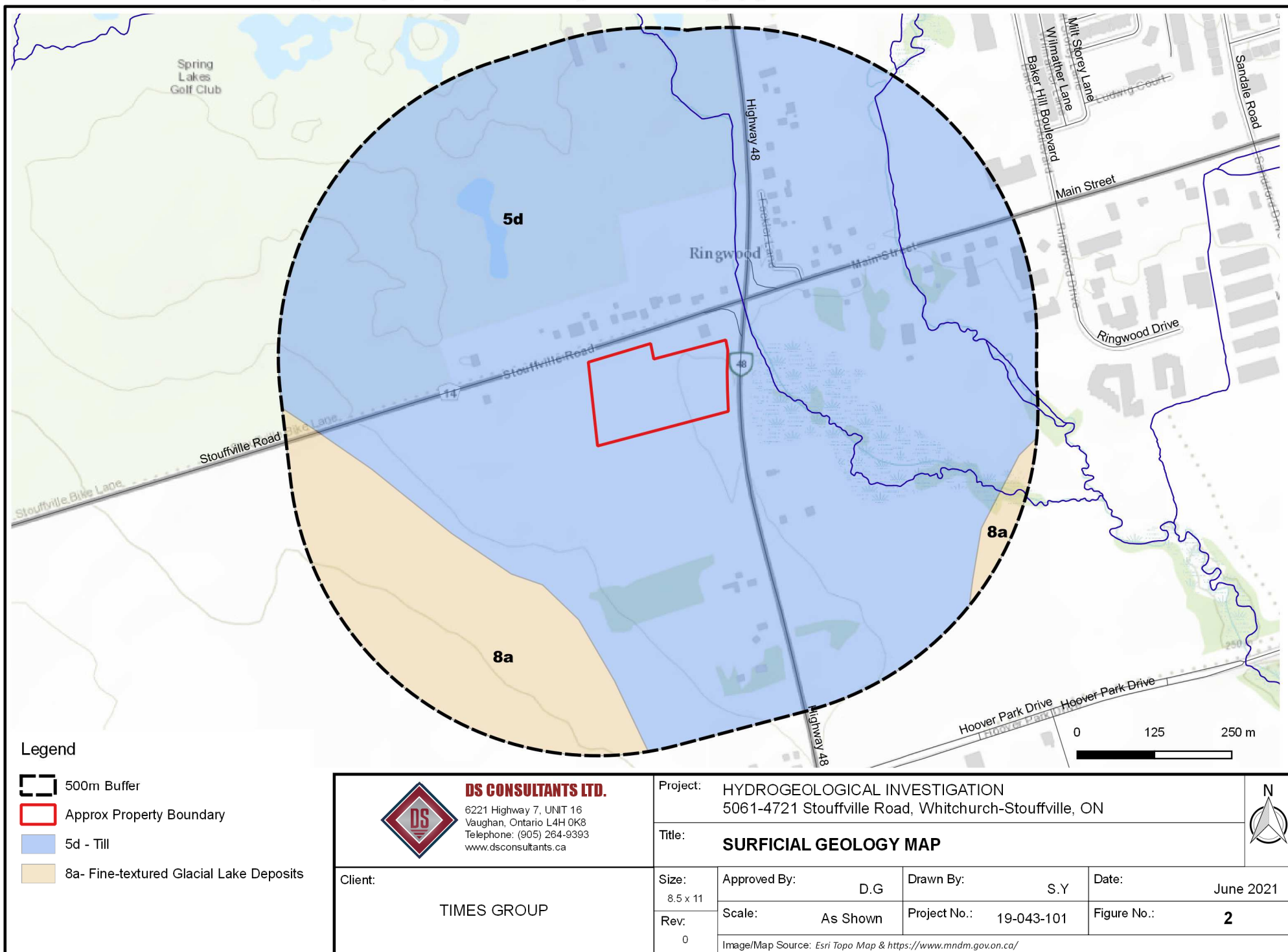
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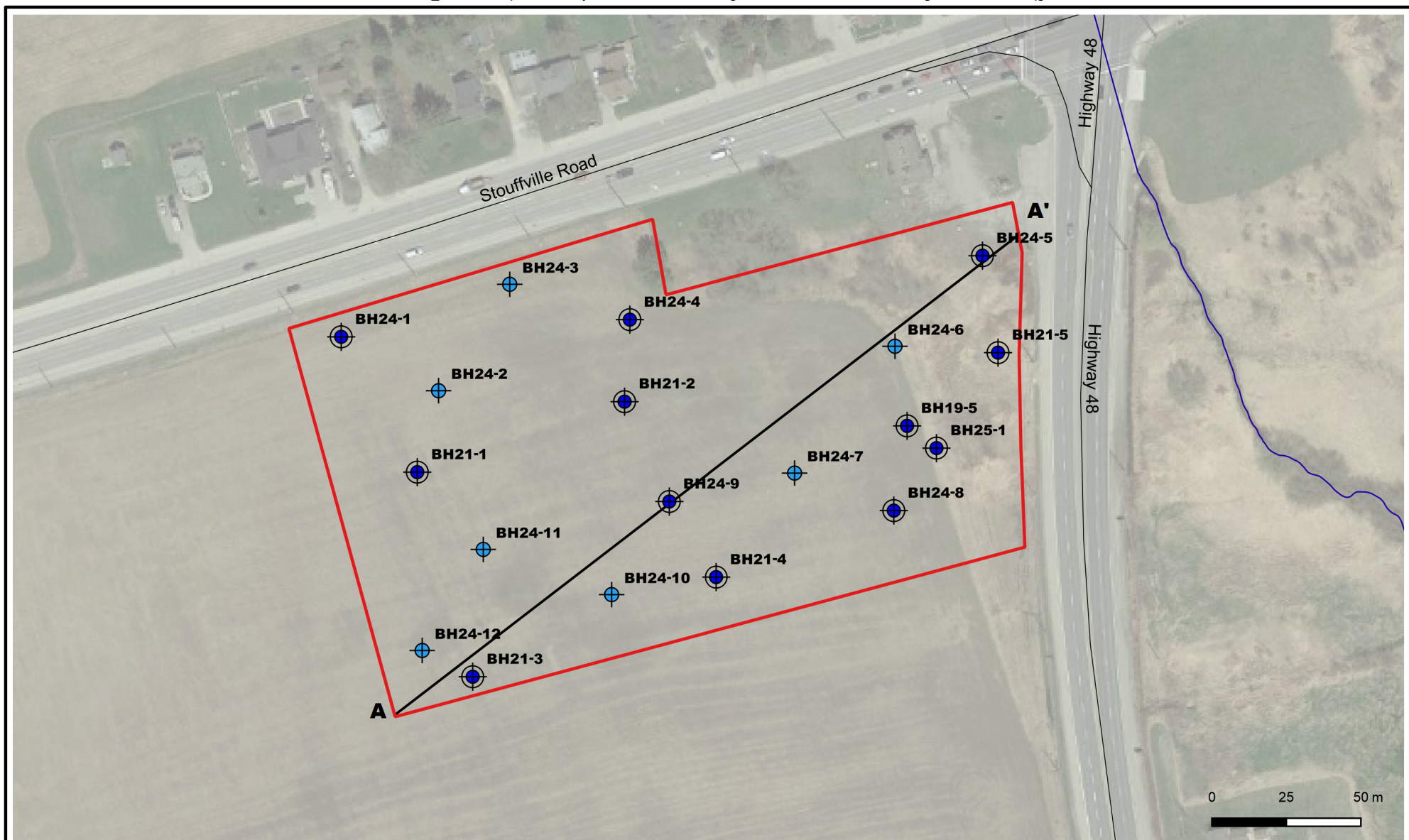
Project No.: **19-043-101**

Figure No.: **1**

Image/Map Source: *Google Satellite Image*







Legend

- Approx Property Boundary
- Cross Section
- Borehole
- Monitoring Well



DS CONSULTANTS LTD.

6221 Highway 7, UNIT 16
Vaughan, Ontario L4H 0K8
Telephone: (905) 264-9393
www.dsconsultants.ca

Client:

TIMES GROUP

Project:

HYDROGEOLOGICAL INVESTIGATION
5061-4721 Stouffville Road, Whitchurch-Stouffville, ON

Title:

BOREHOLE AND MONITORING WELL LOCATIONS

Size:
8.5 x 11

Rev:
0

Approved By:

D.S

Drawn By:

S.Y

Date:

April 2025

Scale:

As Shown

Project No.:

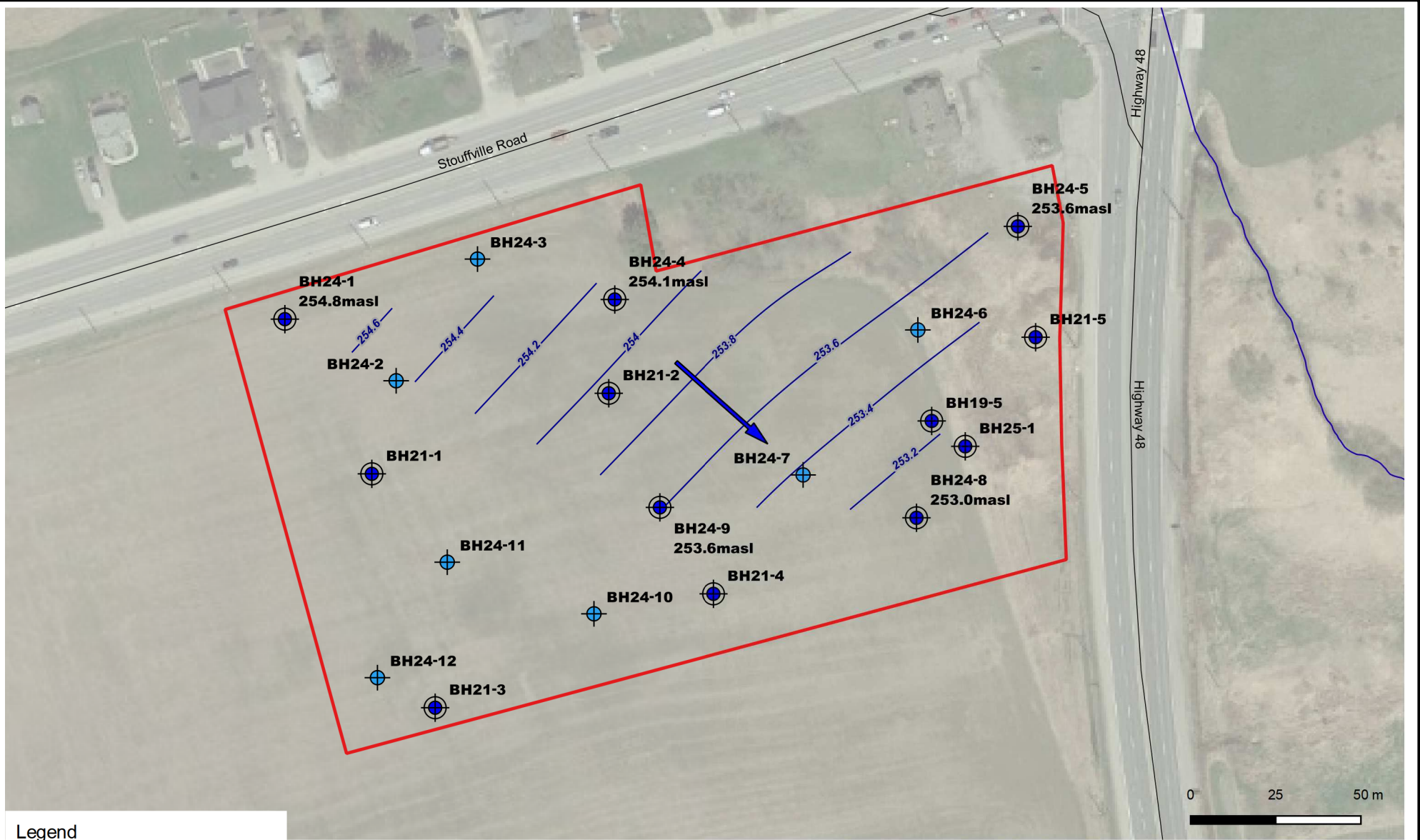
19-043-101

Figure No.:



3

Image/Map Source: Google Satellite Image

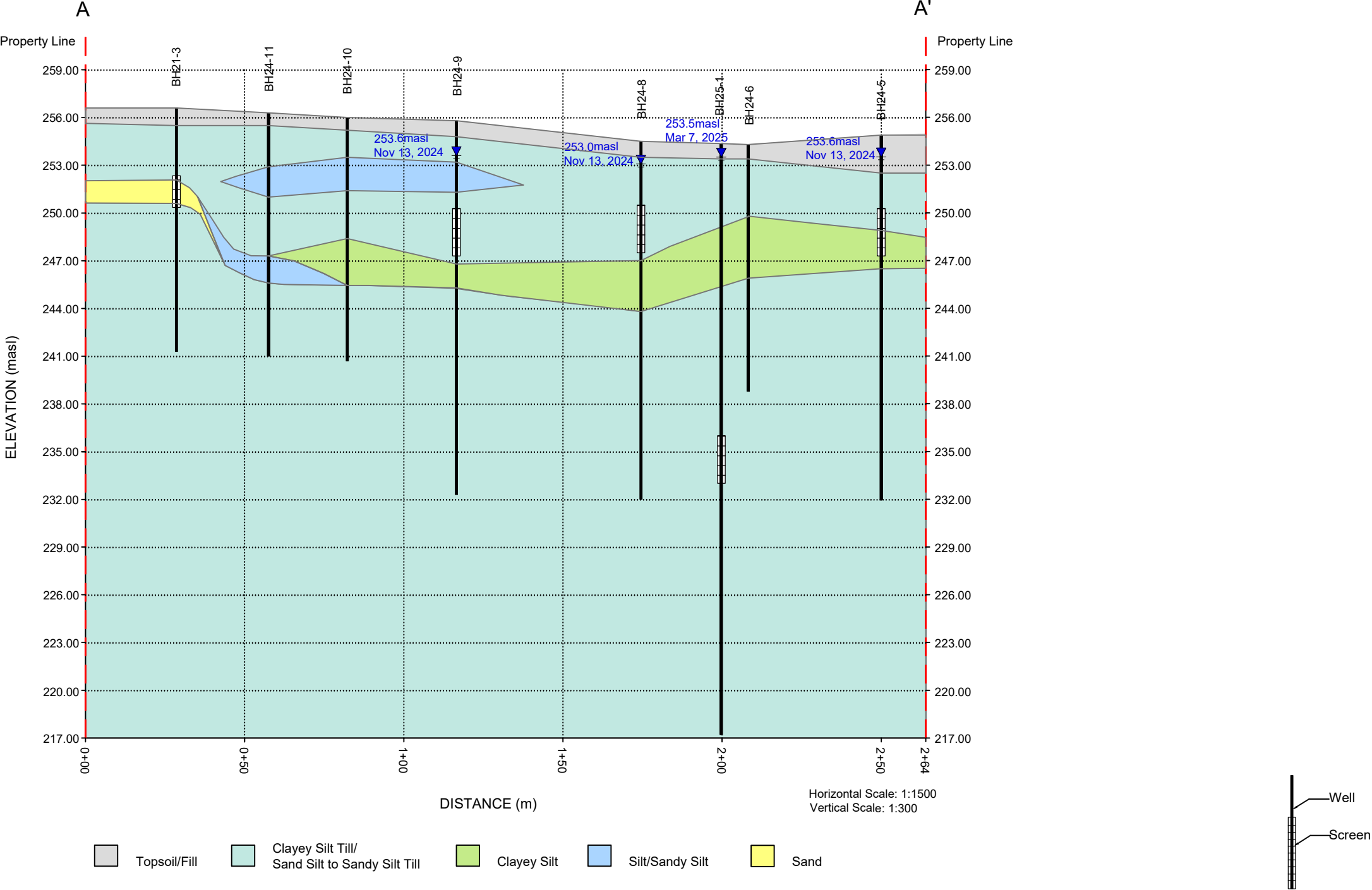





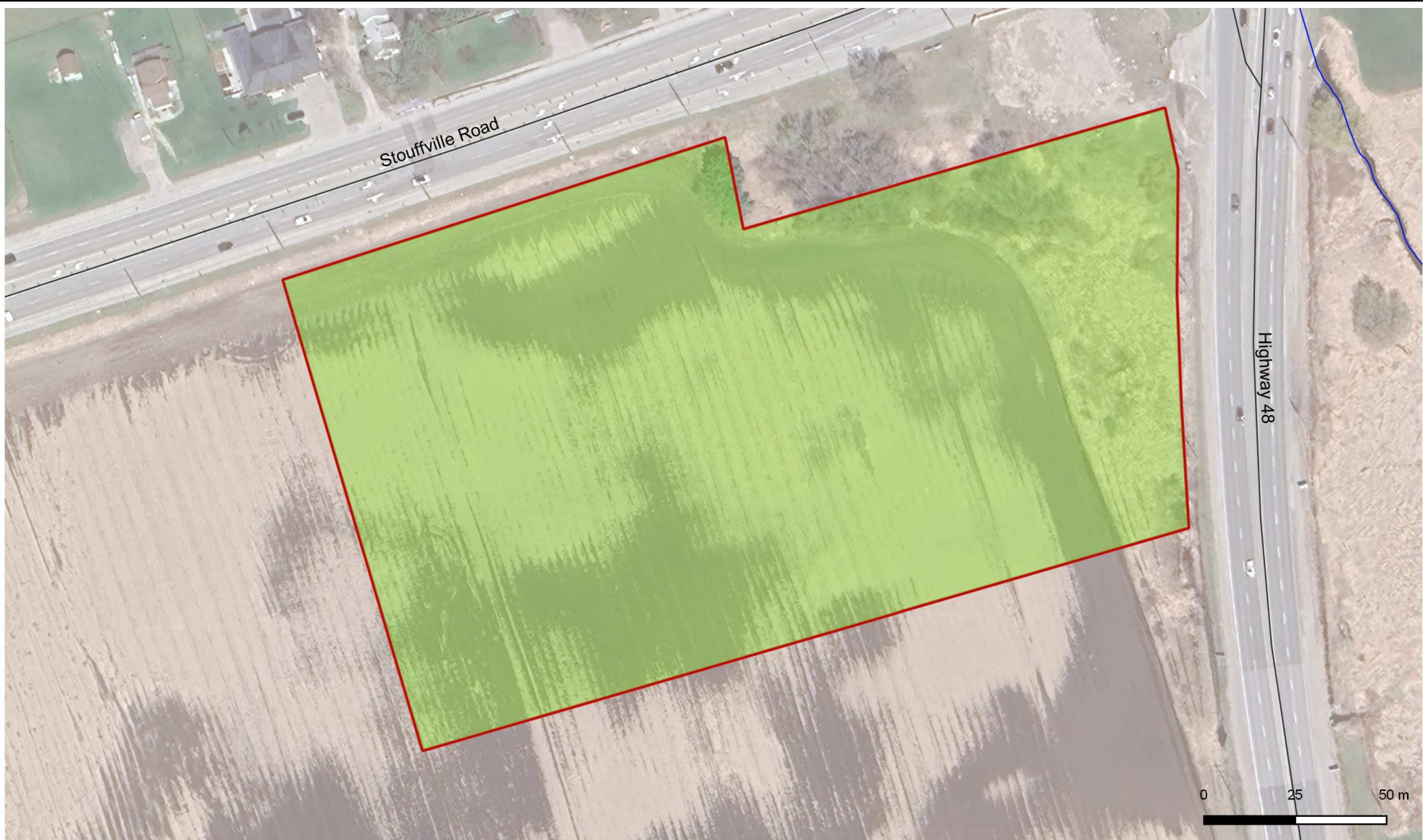
- Legend
- Approx Property Boundary
 - ⊕ Borehole
 - ⊗ Monitoring Well
 - ➔ Groundwater Flow Direction
 - Groundwater Elevation Contour (Nov 13, 2024)

<div><div>DS CONSULTANTS LTD. 6221 Highway 7, UNIT 16 Vaughan, Ontario L4H 0K8 Telephone: (905) 264-9393 www.dsconsultants.ca</div></div>	Project: HYDROGEOLOGICAL INVESTIGATION 5061-4721 Stouffville Road, Whitchurch-Stouffville, ON			
	Title: INFERRED GROUNDWATER CONTOURS AND FLOW DIRECTION MAP			
Client: TIMES GROUP	Size: 8.5 x 11	Approved By: D.S	Drawn By: S.Y	Date: April 2025
	Rev: 0	Scale: As Shown	Project No.: 19-043-101	Figure No.: 4
		Image/Map Source: <i>Google Satellite Image</i>		



Path:j:\gis\2019 projects\19-043-100 4721 and 5061 stouffville road_times group\7-misc\cad\geological cross section - ne.dwg



 <div>DS CONSULTANTS LTD. 6221 Highway 7, UNIT 16 Vaughan, Ontario L4H 0K8 Telephone: (905) 264-9393 www.dsconsultants.ca</div>	Project: HYDROGEOLOGICAL INVESTIGATION 5061-4721 Stouffville Road, Whitchurch-Stouffville, ON			
	Title: GEOLOGICAL CROSS SECTION A-A'			
Client: TIMES GROUP		Size: 11 X 17	Approved By: D.S	Drawn By: S.Y
		Rev.	Scale: As Shown	Date: April 2025
		Project No: 19-043-101		Figure No. 5





- Legend
- Approx Property Boundary
 - Agricultural and Open Space

<div><div>DS CONSULTANTS LTD. 6221 Highway 7, UNIT 16 Vaughan, Ontario L4H 0K8 Telephone: (905) 264-9393 www.dsconsultants.ca</div></div>	Project: HYDROGEOLOGICAL INVESTIGATION 5061-4721 Stouffville Road, Whitchurch-Stouffville, ON			
	Title: PRE DEVELOPMENT LANDUSE			
Client: TIMES GROUP	Size: 8.5 x 11	Approved By: D.G	Drawn By: S.Y	Date: December 2024
	Rev: 0	Scale: As Shown	Project No.: 19-043-100	Figure No.: 6A
		Image/Map Source: <i>Google Satellite Image</i>		



- Legend
- Approx Property Boundary
 - Building
 - Open Space
 - Road/Driveway/Parking

<div><div>DS CONSULTANTS LTD. 6221 Highway 7, UNIT 16 Vaughan, Ontario L4H 0K8 Telephone: (905) 264-9393 www.dsconsultants.ca</div></div>	Project: HYDROGEOLOGICAL INVESTIGATION 5061-4721 Stouffville Road, Whitchurch-Stouffville, ON			
	Title: POST DEVELOPMENT LANDUSE			
Client: TIMES GROUP	Size: 8.5 x 11	Approved By: D.G	Drawn By: S.Y	Date: December 2024
	Rev: 0	Scale: As Shown	Project No.: 19-043-100	Figure No.: 6B
	Image/Map Source: <i>Google Satellite Image</i>			



Appendix A

PROJECT: Preliminary Geotechnical Investigation

CLIENT: Times Group Corp

PROJECT LOCATION: 4721 to 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BOREHOLE LOCATION: See Drawing 1 N 4869147.9 E 637851

DRILLING DATA

Method: Solid Stem Auger

Diameter: 150mm

Date: May/01/2019

REF. NO.: 19-043-100

ENCL NO.: 6

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	DYNAMIC CONE PENETRATION RESISTANCE PLOT				POCKET PEN (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	METHANE AND GRAIN SIZE DISTRIBUTION (%)						
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m		SHEAR STRENGTH (kPa)							WATER CONTENT (%)					
ELEV DEPTH							○ UNCONFINED + FIELD VANE & Sensitivity ● QUICK TRIAXIAL × LAB VANE							W _p	W	W _L			
254.3							20	40	60	80	100								
254.0	TOPSOIL: 125mm		1	SS	5														
253.5	FILL: silty clay, trace sand, brown, moist, firm																		
0.8	SANDY SILT TILL: trace to some clay, some gravel, occasional cobble/boulder, brown, wet, compact to very dense		2	SS	10														
			3	SS	14														
			4	SS	78														
	some clay, grey, moist below 3.1m		5	SS	94														
			6	SS	86														
248.2	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, hard		7	SS	40														
246.7	SILT TO SANDY SILT: some clay, grey, moist, dense		8	SS	46														
245.2	CLAYEY SILT TILL: sandy, trace gravel/ cobble, grey, moist, hard		9	SS	36														
			10	SS	47														
242.1	SILTY SAND TO SANDY SILT TILL: trace to some clay, trace cobbles, grey, moist, very dense		11	SS	86														
241.0	SAND AND GRAVEL: trace silt, grey, wet, dense		12	SS	39														
239.1	END OF BOREHOLE																		
15.2	Notes: 1) 50mm dia. monitoring well installed at 15.2 mbgl upon completion. 2) Water level readings: Date: May 23, 2019 W.L. Depth (m): -0.30 (above ground surface)																		

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG 19-043-100, 4271 STOUFFVILLE GPJ DS.GDT 7/16/19

PROJECT: Geotechnical Investigation - Additional Work

CLIENT: Times Group

PROJECT LOCATION: 4721 and 5061 Stouffville Rd, Whitchurch-Stouffville, ON

DATUM: Geodetic

BOREHOLE LOCATION: See Drawing 1 N 4869159.459 E 637854.913

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Feb-11-2021

REF. NO.: 19-043-101

ENCL NO.: 8

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN. (Cu) (MPa)	NATURAL UNIT WT (kN/m ³)	METHANE AND GRAIN SIZE DISTRIBUTION (%)			
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m		ELEVATION	SHEAR STRENGTH (kPa)								WATER CONTENT (%)			
254.5								20	40	60	80	100							
254.0	TOPSOIL: 300mm		1	SS	7		W. L. 254.1 m Feb 21, 2025												
0.3	CLAYEY SILT: some sand, trace gravel, brown, moist, firm (weathered)		2	SS	17														
253.7																			
250.8	SILTY SAND: trace clay, trace gravel, brown, wet, compact		3	SS	17		W. L. 253.1 m Apr 13, 2021												
1.0	SANDY SILT TILL: trace clay, trace gravel, brown, moist, compact to dense		4	SS	20														
			5	SS	36														
	grey below 4.5m		6	SS	31														
248.5																			
6.0	CLAYEY SILT TILL: some sand, trace gravel, grey, moist, very stiff		7	SS	25														
			8	SS	19														
			9	SS	17														
			10	SS	22														
242.3																			
12.2	SAND AND GRAVEL: silty, trace cobble, trace clay, grey, saturated, compact		11	SS	29														
240.8																			
13.7	SILTY SAND TILL: trace clay, trace gravel, brown, wet, compact to very dense		12	SS	21														
238.7			13	SS	52														
15.8	END OF BOREHOLE																		
	Notes: 1) 50mm dia. monitoring well installed upon completion. 2) Water level readings:																		
	Date: April 13, 2021	W.L. Depth (m): 1.37																	
	Feb. 25, 2021	0.4																	

DS SOIL LOG 19-043-101 4721 AND 5061 STOUFFVILLE RD ADDITIONAL WORK_TIMES GROUP.GPJ DS.GDT 21-5-3

GROUNDWATER ELEVATIONS

	1st	2nd	3rd	4th
Measurement				

GRAPH
NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ $\epsilon = 3\%$ Strain at Failure

PROJECT: Geotechnical Investigation - Additional Work

CLIENT: Times Group

PROJECT LOCATION: 4721 and 5061 Stouffville Rd, Whitchurch-Stouffville, ON

DATUM: Geodetic

BOREHOLE LOCATION: See Drawing 1 N 4869127.615 E 637803.503

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Feb-11-2021

REF. NO.: 19-043-101

ENCL NO.: 9

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	METHANE AND GRAIN SIZE DISTRIBUTION (%)						
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)									WATER CONTENT (%)			GR	SA	SI	CL
ELEV DEPTH								○ UNCONFINED ● QUICK TRIAXIAL	+ FIELD VANE & Sensitivity × LAB VANE	20	40						60	80	100				
255.2							W. L. 255.2 m Feb 21, 2025																
254.9	TOPSOIL: 300mm		1	SS	13																		
254.4	SANDY SILT: trace clay, trace gravel, trace organics, brown, moist, compact (weathered)		2	SS	14																		
254.1	CLAYEY SILT TILL: sandy, trace gravel/ cobble, grey, moist, stiff to hard		3	SS	24		W. L. 254.1 m Apr 13, 2021																
253.0	No recovery at 2.3m		4	SS	60																		
252.2	SANDY SILT TILL: clay seams, trace gravel/ cobble, grey, moist, dense to very dense		5	SS	37																		
251.0	some clay below 4.5m		6	SS	33																		
249.0			7	SS	58																		
247.7	CLAYEY SILT TILL: some sand to sandy, trace gravel/ cobble, grey, moist, very stiff to hard		8	SS	25																		
246.0			9	SS	30																		
244.5	SANDY SILT TILL: some clay, trace gravel/ cobble, grey, wet, compact		10	SS	15																		
243.0	SAND: trace clay, trace gravel, grey, saturated		11	SS	disturbed																		
241.5	SANDY SILT TILL: trace clay, trace gravel/ cobble, grey, moist, very dense		12	SS	50/ 25mm																		
239.7	END OF BOREHOLE		13	SS	50/ 100mm																		
15.5	Notes: 1) 50mm dia. monitoring well installed upon completion. 2) Water level readings: Date: W.L. Depth (m): April 13, 2021 1.18 Feb. 25, 2021 - 0.02 (above ground)																						

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG 19-043-101 4721 AND 5061 STOUFFVILLE RD ADDITIONAL WORK TIMES GROUP GPJ DS GDT 21-5-3

PROJECT: Geotechnical Investigation - Additional Work

CLIENT: Times Group

PROJECT LOCATION: 4721 and 5061 Stouffville Rd, Whitchurch-Stouffville, ON

DATUM: Geodetic

BOREHOLE LOCATION: See Drawing 1 N 4869091.791 E 637696.023

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Feb-16-2021

REF. NO.: 19-043-101

ENCL NO.: 10

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID		POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	METHANE AND GRAIN SIZE DISTRIBUTION (%)	
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		W _p	W				W _L
ELEV DEPTH								○ UNCONFINED	+ FIELD VANE & Sensitivity	W _p	W				W _L
								● QUICK TRIAXIAL	× LAB VANE	WATER CONTENT (%)					
						20	40	60	80	100	10	20	30		GR SA SI CL
256.6															
0.0	TOPSOIL: 380mm		1	SS	21		256								
256.2															
0.4	CLAYEY SILT: trace clay, trace gravel, trace topsoil, dark brown, moist, stiff to very stiff (weathered)		2	SS	11		255								
255.5															
1.1	CLAYEY SILT TILL: sandy, trace gravel, sand seams, brown, moist, stiff		3	SS	11		255								
254.3															
2.3	SANDY SILT TILL: some clay, trace gravel/ cobbles, brown, moist, compact to dense		4	SS	22		254								
252.1															
4.5	SAND: some silt, trace clay, brown, saturated		5	SS	36		252								
250.6															
6.0	CLAYEY SILT TILL: sandy, trace gravel, sand seams, grey, moist, very stiff to hard		6	SS	86/230mm		251								
245.9															
10.7	SANDY SILT TO SILTY SAND TILL: trace clay, trace gravel, grey, wet, dense to very dense		7	SS	86/280mm		250								
241.3															
15.3	END OF BOREHOLE Notes: 1) 50mm dia. monitoring well installed upon completion. 2) Water level readings: Date: April 13, 2021 Feb. 25, 2021		8	SS	24		249								
							</								

PROJECT: Geotechnical Investigation - Additional Work

CLIENT: Times Group

PROJECT LOCATION: 4721 and 5061 Stouffville Rd, Whitchurch-Stouffville, ON

DATUM: Geodetic

BOREHOLE LOCATION: See Drawing 1 N 4869153.844 E 637681.724

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Feb-12-2021

REF. NO.: 19-043-101

ENCL NO.: 11

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	METHANE AND GRAIN SIZE DISTRIBUTION (%)					
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)							WATER CONTENT (%)				
ELEV DEPTH								○ UNCONFINED + FIELD VANE & Sensitivity ● QUICK TRIAXIAL × LAB VANE							W _p	W	W _L		
256.7								20	40	60	80	100							
256.4	TOPSOIL AND SILT: 330mm		1	SS	16		W. L. 256.4 m Apr 13, 2021												
255.9	CLAYEY SILT: trace gravel, trace topsoil, brown, moist, very stiff (weathered)		2	SS	15														
255.2	CLAYEY SILT TILL: sandy, trace gravel, brown, moist, very stiff		3	SS	18		255												
253.7	SANDY SILT TILL: trace clay, trace gravel/ cobble, brown, very moist, compact		4	SS	22		W. L. 254.8 m Feb 21, 2025												
253.7			5	SS	36		254												
252.2							253												
252.2	CLAYEY SILT TILL: some sand, trace gravel, grey, moist, very stiff to hard		6	SS	20		252												
							251												
			7	SS	34		250											3	16
							249											54	27
			8	SS	45		248												
							247												
			9	SS	47		246												
246.0	SANDY SILT TILL: some clay, trace gravel/ cobble, grey, very moist, very dense		10	SS	50/25mm		245												
244.4																			
12.3	END OF BOREHOLE Notes: 1) 50mm dia. monitoring well installed upon completion. 2) Water level readings: Date: April 13, 2021 Feb. 25, 2021		11	SS	50/25mm														
	W.L. Depth (m): 0.28 1.9																		

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG 19-043-101 4721 AND 5061 STOUFFVILLE RD ADDITIONAL WORK TIMES GROUP GPJ DS GDT 21-5-3

PROJECT: Geotechnical Investigation - Additional Work

CLIENT: Times Group

PROJECT LOCATION: 4721 and 5061 Stouffville Rd, Whitchurch-Stouffville, ON

DATUM: Geodetic

BOREHOLE LOCATION: See Drawing 1 N 4869178.503 E 637758.266

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Feb-12-2021

REF. NO.: 19-043-101

ENCL NO.: 12

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	METHANE AND GRAIN SIZE DISTRIBUTION (%) GR SA SI CL			
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)										WATER CONTENT (%)		
ELEV DEPTH								○ UNCONFINED	● QUICK TRIAXIAL	○ FIELD VANE & Sensitivity	× LAB VANE							W _P	W	W _L
								20	40	60	80							100	10	20
255.6							W. L. 255.6 m													
255.0	0.3	TOPSOIL: 330mm				1	SS	9												
		CLAYEY SILT: trace sand, trace topsoil, brown, moist, stiff (weathered)																		
254.5						2	SS	16												
	1.1	CLAYEY SILT TILL: sandy, trace gravel/ cobble, grey, moist, very stiff to hard																		
						3	SS	15												
		grey below 2.7m				4	SS	43												
						5	SS	21												
		sand seams below 4.5m																		
						6	SS	26												
						7	SS	25												
						8	SS	20												
246.6	9.0	SANDY SILT TILL: some clay, trace gravel/ cobble, grey, moist, very dense				9	SS	50/50mm												
244.9	244.7	SAND: some silt, trace clay, trace gravel, brown, wet, very dense				10	SS	94/280mm												
	10.9	SANDY SILT TILL: trace clay, trace gravel, grey, moist, very dense																		
243.1						11	SS	50/25mm												
12.5		END OF BOREHOLE Notes: 1) 50mm dia. monitoring well installed upon completion. 2) Water level readings: Date: April 13, 2021 Feb. 25, 2021 W.L. Depth (m): 0.30 - 0.02 (above ground)																		

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3, x 3: Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG 19-043-101 4721 AND 5061 STOUFFVILLE RD ADDITIONAL WORK, TIMES GROUP GPJ DS GDT 21-5-3



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869173.7 E 637660.6

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Oct-24-2024

REF. NO.: 19-043-103

ENCL NO.: 2

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT MOISTURE CONTENT LIMIT			POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		W _p	W	W _L			
256.6								20 40 60 80 100							GR SA SI CL
256.0	TOPSOIL: 270mm		1	SS	11			20 40 60 80 100							
0.3	FILL: sandy silt, trace rootlets, trace gravel, dark brown to brown, moist, compact		2	SS	14			20 40 60 80 100							
255.8	FILL: clayey silt, sandy, trace organics, trace cobble, dark brown to brown, moist, stiff		3	SS	21			20 40 60 80 100							
255.0	SANDY SILT TILL: trace to some clay, trace gravel, occasional cobble, brown, moist, compact to dense clayey silt till layer at 2.6m		4	SS	34			20 40 60 80 100							
253.6	SILTY SAND: trace clay, brown, wet, dense		5	SS	34			20 40 60 80 100							
252.1	SILTY CLAY TILL: sandy, trace gravel, occasional cobble, grey, moist, hard		6	SS	75			20 40 60 80 100							
249.1	CLAYEY SILT: trace sand, grey, moist, hard		8	SS	39			20 40 60 80 100							
247.6	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, occasional cobble, grey, moist to very moist, very dense		9	SS	50/ 30mm			20 40 60 80 100							
			10	SS	50/ 30mm			20 40 60 80 100							
			11	SS	50/ 30mm			20 40 60 80 100							
			12	SS	50/ 30mm			20 40 60 80 100							
			13	SS	50/ 30mm			20 40 60 80 100							
			14	SS	50/ 30mm			20 40 60 80 100							

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH
NOTES+ 3 , × 3 : Numbers refer
to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS GDT 24-11-27

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

REF. NO.: 19-043-103

Date: Oct-24-2024

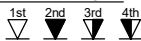
ENCL NO.: 2

BH LOCATION: See Drawing 1 N 4869173.7 E 637660.6

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%) GR SA SI CL		
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)								WATER CONTENT (%)	
								20	40							60	80

GROUNDWATER ELEVATIONS

Measurement



GRAPH
NOTES

$+^3, \times^3$: Numbers refer to Sensitivity

○ **ε**=3% Strain at Failure

PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869156.4 E 637693.6

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Oct-28-2024

REF. NO.: 19-043-103

ENCL NO.: 3

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				POCKET PEN (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)				
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)							WATER CONTENT (%)			
								○ UNCONFINED	● QUICK TRIAXIAL	+ FIELD VANE & Sensitivity	× LAB VANE				W _P	W	W _L	
256.3							20	40	60	80	100	10	20	30	GR	SA	SI	CL
256.0	TOPSOIL: 270mm		1	SS	9													
0.3	FILL: clayey silt, trace rootlets, trace organics, trace gravel, dark brown to brown, moist, stiff																	
255.3	CLAYEY SILT TILL: sandy, trace gravel, brown, moist, stiff to very stiff		2	SS	10													
1.0			3	SS	10													
	silt layer at 2.3m		4	SS	23													
253.3	SILT: trace to some clay, trace sand, brown, wet, dense		5	SS	36													
3.0																		
251.7																		
251.6	SAND: trace silt, trace clay, grey, wet, dense		6	SS	31													
4.8	CLAYEY SILT TILL: sandy, trace gravel, occasional cobble, grey, moist, hard		7	SS	50/ 100mm													
	silt layer at 7.6m		8	SS	33													
			9	SS	50/ 130mm													
245.8	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, grey, very moist, very dense silt layer at 10.7m		10	SS	50/ 130mm													
10.5																		
			11	SS	50/ 100mm													
			12	SS	50/ 130mm													
240.8	END OF BOREHOLE:		13	SS	50/ 100mm													
15.5	Notes: 1) Water encountered at 3.0m during drilling.																	

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869192.4 E 637716.7

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Oct-26-2024

REF. NO.: 19-043-103

ENCL NO.: 4

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)		
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)								WATER CONTENT (%)	
								○ UNCONFINED ● QUICK TRIAXIAL	+ FIELD VANE & Sensitivity × LAB VANE								
256.2							20 40 60 80 100								GR SA SI CL		
256.0	TOPSOIL: 250mm		1	SS	8												
0.3	FILL: sandy silt, trace rootlets, trace gravel, dark brown to brown, moist, loose to compact																
255.3	CLAYEY SILT TILL: sandy, trace gravel, occasional cobble, brown, moist, very stiff		2	SS	15												
0.9																	
			3	SS	17												
2																	
253.8	SILT: trace to some clay, trace sand, brown, moist to wet, dense		4	SS	37												
2.4																	
253.2	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, stiff to hard		5	SS	12												
3.0																	
			6	SS	30												
4																	
			7	SS	26												
6																	
248.7	CLAYEY SILT: trace sand, grey, moist, very stiff		8	SS	26												
7.5																	
247.2	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, occasional cobble, grey, moist to very moist, very dense		9	SS	50/ 100mm												
9.0																	
			10	SS	50/ 130mm												
10																	
			11	SS	50/ 100mm												
11																	
			12	SS	50/ 130mm												
12																	
			13	SS	50/ 130mm												
13																	

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH
NOTES+ 3 , × 3 : Numbers refer
to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27

PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869192.4 E 637716.7

DRILLING DATA

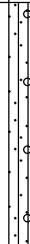
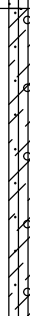
Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm





Date: Oct-26-2024

REF. NO.: 19-043-103

ENCL NO.: 4

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			POCKET PEN (Cu) (MPa)	NATURAL UNIT WT (kN/m³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)				
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			20 40 60 80 100	20 40 60 80 100	W _P W W _L	20 40 60 80 100	10 20 30	GR SA SI CL									
	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, occasional cobble, grey, moist to very moist, very dense(Continued)				75mm		239															
			15	SS	50/ 50mm		238															
								237														
236.4	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, hard		16	SS	50/ 100mm		236															
19.8							235															
			17	SS	50/ 130mm		234															
								233														
232.8	END OF BOREHOLE: Notes: 1) Water encountered at 2.4m during drilling.		18	SS	50/ 130mm		233									6 39 39 16						
23.4																						

GROUNDWATER ELEVATIONS

	1st	2nd	3rd	4th
Measurement				

GRAPH
NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ $\epsilon = 3\%$ Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27

PROJECT: Geotechnical Investigation
CLIENT: Times Group Corporation
PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON
DATUM: Geodetic
BH LOCATION: See Drawing 1 N 4869181.5 E 637757.2

DRILLING DATA
Method: Hollow Stem Auger
Diameter: 200mm
Date: Oct-28-2024
REF. NO.: 19-043-103
ENCL NO.: 5

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT		POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			20 40 60 80 100	20 40 60 80 100	W _p	W	W _L		
255.4														GR SA SI CL
255.0	TOPSOIL: 250mm		1	SS	10		255							
0.3	FILL: clayey silt, trace rootlets, trace organics, trace gravel, dark brown to brown, moist, stiff to very stiff		2	SS	20		254.4							
254.4	CLAYEY SILT TO SILTY CLAY TILL: sandy, trace gravel, brown, moist, stiff to hard		3	SS	13		254							
1.0			4	SS	42		253							
			5	SS	26		252							
	grey below 3.0 m		6	SS	32		251							
			7	SS	54		250							
			8	SS	19		249							
	silt layer at 6.1 m		9	SS	50/30mm		248							
			10	SS	81		247							
246.4	SANDY SILT TILL: trace to some clay, trace gravel, occasional cobble, grey, moist, very dense		11	SS	50/30mm		246							
9.0			12	SS	50/30mm		245							
			13	SS	50/30mm		244							
243.4	CLAYEY SILT TILL: sandy, trace gravel, occasional cobble, grey, moist, hard		14	SS	50/30mm		243							
12.0			15	SS	50/30mm		242							
			16	SS	50/30mm		241							
239.9	END OF BOREHOLE:		17	SS	50/30mm		240							
15.5	Notes: 1) 50mm dia. monitoring well installed upon completion. 2) Water Level Readings:													

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

REF. NO.: 19-043-103

Date: Oct-28-2024

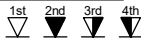
ENCL NO.: 5

BH LOCATION: See Drawing 1 N 4869181.5 E 637757.2

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GROUNDWATER ELEVATIONS

Measurement



GRAPH
NOTES

$+^3, \times^3$: Numbers refer to Sensitivity

○ **$\epsilon = 3\%$** Strain at Failure



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869205.3 E 637875.1

DRILLING DATA

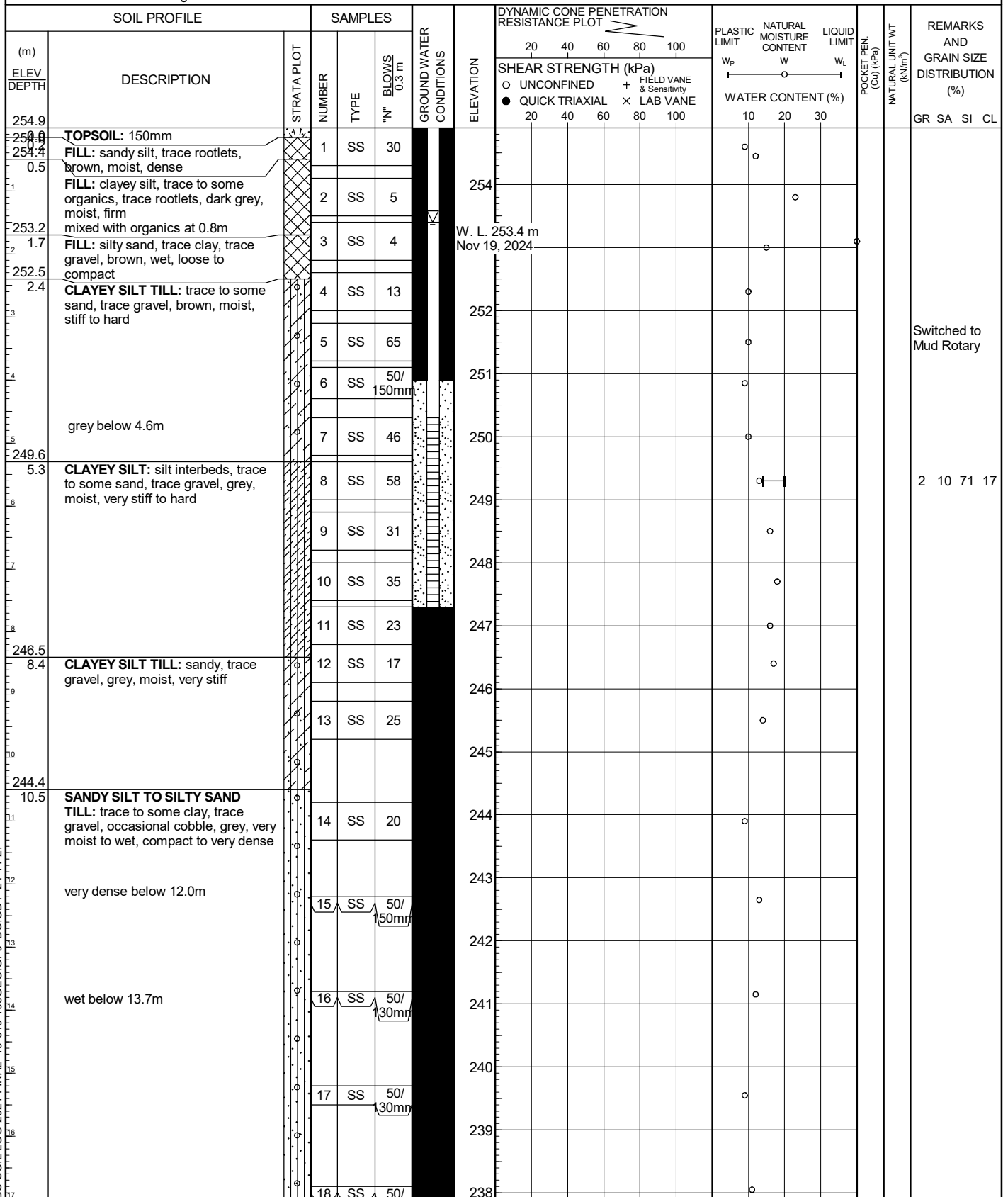
Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Nov-05-2024

REF. NO.: 19-043-103

ENCL NO.: 6



DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869205.3 E 637875.1

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Nov-05-2024

REF. NO.: 19-043-103

ENCL NO.: 6

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT CONTENT			POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)				W _p	W	W _L			
								20 40 60 80 100									GR SA SI CL
	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, occasional cobble, grey, very moist to wet, compact to very dense(Continued) gravelly at 18.3m				30mm												
18			19	SS	50/ 75mm		237										
19							236										
20			20	SS	50/ 100mm		235										
21							234										
233.6							234										
21.3	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, hard		21	SS	50/ 30mm		233										
22							233										
231.9							232										
23.0	END OF BOREHOLE: Notes: 1) 50mm dia. monitoring well installed beside original location. 2) Water Level Readings: Date: Water Level(mbgl): Nov. 19, 2024 1.5		22	SS	50/ 100mm		232										

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH
NOTES

+ 3 , × 3 : Numbers refer
to Sensitivity

○ = 3% Strain at Failure



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869174.4 E 637846.4

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Oct-31-2024

REF. NO.: 19-043-103

ENCL NO.: 7

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)				
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)							WATER CONTENT (%)			
								○ UNCONFINED		+ FIELD VANE & Sensitivity					W _p	W	W _L	
								● QUICK TRIAXIAL		× LAB VANE								
254.4							20	40	60	80	100	10	20	30	GR	SA	SI	CL
254.0	TOPSOIL: 230mm		1	SS	7													
0.2	FILL: clayey silt, trace rootlets, trace organics, trace gravel, dark brown to brown, moist, firm																	
253.5			2	SS	19													
0.9	CLAYEY SILT TILL: sandy, trace gravel, occasional cobble, brown, moist, very stiff to hard																	
			3	SS	21													
			4	SS	24													
	grey below 3.1m		5	SS	35													
			6	SS	18													
249.9			7	SS	17													
4.5	CLAYEY SILT: frequent silt layers, trace sand, grey, moist, stiff to very stiff		8	SS	11													
			9	SS	12													
	trace gravel below 6.1m		10	SS	26													
			11	SS	21													
246.0			12	SS	19													
8.4	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, very stiff		13	SS	17													
243.9			14	SS	20													
10.5	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, grey, very moist to wet, compact to very dense																	
			15	SS	63													
			16	SS	17													
	wet at 13.7m																	
239.0			17	SS	50/ 75mm													
15.4	END OF BOREHOLE: Notes: 1) Water encountered at 4.0m during drilling.																	

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ = 3% Strain at Failure

PROJECT: Geotechnical Investigation
CLIENT: Times Group Corporation
PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON
DATUM: Geodetic
BH LOCATION: See Drawing 1 N 4869131.3 E 637813.6

DRILLING DATA
Method: Hollow Stem Auger
Diameter: 200mm
Date: Nov-01-2024
REF. NO.: 19-043-103
ENCL NO.: 8

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT		POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			20 40 60 80 100	20 40 60 80 100	W _p W W _L	WATER CONTENT (%)			
254.8	TOPSOIL: 250mm													GR SA SI CL
254.0	FILL: clayey silt, trace rootlets, trace organics, trace gravel, dark brown to brown, moist, stiff		1	SS	8		254							
253.9	CLAYEY SILT TILL: sandy, trace gravel, occasional cobble, brown, moist, stiff to hard		2	SS	13		253							
			3	SS	17		252							
			4	SS	52		251							
			5	SS	36		250							
251.0	SANDY SILT TILL: trace to some clay, trace gravel, brown to grey, moist, very dense		6	SS	50/130mm		249							
250.3	CLAYEY SILT TILL: sandy, frequent silt pockets, trace gravel, occasional cobble, grey, moist, very stiff to hard		7	SS	49		248							
			8	SS	27		247							
			9	SS	54		246							
			10	SS	26		245							
			11	SS	24		244							
			12	SS	22		243							
			13	SS	25		242							
			14	SS	disturbed		241							
242.8	SAND: some gravel, trace silt, trace clay, grey, wet, very dense		15	SS	69		240							15 73 9 1
241.3	SANDY SILT TILL: trace to some clay, trace gravel, grey, very moist, very dense		16	SS	63									
239.3	END OF BOREHOLE:		17	SS	50/									
15.5	Notes: 1) Water encountered at 3.8 m during drilling.													

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869119.5 E 637847.1

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Oct-30-2024

REF. NO.: 19-043-103

ENCL NO.: 9

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)							
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)								W _P W W _L						
								20 40 60 80 100								10 20 30						
								○ UNCONFINED + FIELD VANE & Sensitivity														
					● QUICK TRIAXIAL × LAB VANE					WATER CONTENT (%)												
254.5															GR SA SI CL							
254.0																						
0.3																						
253.5																						
1.0																						
									</													

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH
NOTES

+ 3 , × 3 : Numbers refer
to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL_19-043-103GEO.GPJ DS.GDT 24-11-27

PROJECT: Geotechnical Investigation
CLIENT: Times Group Corporation
PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON
DATUM: Geodetic
BH LOCATION: See Drawing 1 N 4869119.5 E 637847.1

DRILLING DATA
Method: Hollow Stem Auger/Mud Rotary
Diameter: 200mm
Date: Oct-30-2024
REF. NO.: 19-043-103
ENCL NO.: 9

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC NATURAL LIQUID LIMIT			POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)				W _p	W	W _L			
								20	40	60	80	100					GR SA SI CL
18	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, grey, moist, very dense(Continued)		18	SS	50/30mm		237										
19			19	SS	50/100mm		236										
20.0			20	SS	50/30mm		234										
21.3	SILTY SAND TO SANDY SILT TILL: trace clay, trace gravel, grey, moist, very dense		21	SS	50/75mm		233										
22			22	SS	50/130mm		232										
23.4	END OF BOREHOLE: Notes: 1) 50mm dia. monitoring well installed upon completion. 2) Water Level Readings: Date: Water Level(mbgf): Nov. 19, 2024 1.6																

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869120.9 E 637771.7

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Oct-29-2024

REF. NO.: 19-043-103

ENCL NO.: 10

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)							
255.8								20 40 60 80 100							GR SA SI CL
255.8	TOPSOIL: 270mm		1	SS	8										
0.3	FILL: clayey silt, trace rootlets, trace organics, trace gravel, dark brown to brown, moist, stiff														
254.8			2	SS	12										
1.0	CLAYEY SILT TILL: sandy, trace gravel, brown, moist, stiff to hard														
			3	SS	11										
253.2			4	SS	32										
2.6	SILT: trace clay, trace sand, brown to grey, wet, dense														0 9 88 3
			5	SS	31										
251.3															
4.5	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, very stiff to hard		6	SS	25										
			7	SS	34										
			8	SS	30										
246.8															
9.0	CLAYEY SILT: trace sand, silt layers, grey, moist, hard		9	SS	30										
245.3															
10.5	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, occasional cobble, grey, moist to very moist, very dense		10	SS	50/ 30mm										
			11	SS	50/ 30mm										
			12	SS	50/ 30mm										
			13	SS	50/ 100mm										

W. L. 250.8 m
Nov 19, 2024

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH
NOTES+ 3 × 3: Numbers refer
to Sensitivity

○ = 3% Strain at Failure



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869120.9 E 637771.7

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Oct-29-2024

REF. NO.: 19-043-103

ENCL NO.: 10

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT MOISTURE CONTENT LIMIT			POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		W _p W W _L					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
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								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
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								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
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								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
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								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
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								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
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								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					
								20 40 60 80 100		20 40 60 80 100					
								○ UNCONFINED + FIELD VANE & Sensitivity		○ QUICK TRIAXIAL × LAB VANE					

PROJECT: Geotechnical Investigation
CLIENT: Times Group Corporation
PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON
DATUM: Geodetic
BH LOCATION: See Drawing 1 N 4869089.4 E 637753

DRILLING DATA
Method: Hollow Stem Auger/Mud Rotary
Diameter: 200mm
Date: Nov-04-2024
REF. NO.: 19-043-103
ENCL NO.: 11

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT		POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			20 40 60 80 100	20 40 60 80 100	W _p	W	W _L		
256.0	TOPSOIL: 150mm		1	SS	17									GR SA SI CL
255.2	FILL: silty sand, some clay, trace gravel, trace rootlets, dark brown to brown, moist, compact		2	SS	24		255							Switched to Mud Rotary
253.5	CLAYEY SILT TILL: sandy, trace gravel, brown, moist, stiff to very stiff sandy silt pockets at 1.5m		3	SS	14		254							
252.7	SILT: trace to some clay, trace sand, trace gravel, brown, wet, compact to dense		4	SS	19		253							
251.4	SILTY SAND: clayey silt pockets, brown, wet, dense		5	SS	36		252							
248.4	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, very stiff to hard		6	SS	42		251							
245.5			7				250							
242.7			8				249							
240.7			9				248							
237.9			10				247							
235.1			11				246							
232.3			12				245							auger grinding
229.5			13				244							
226.7			14				243							
223.9			15				242							
221.1			16				241							
218.3			17											
215.5			18											
212.7			19											
209.9			20											
207.1			21											
204.3			22											
201.5			23											
198.7			24											
195.9			25											
193.1			26											
190.3			27											
187.5			28											
184.7			29											
181.9			30											
179.1			31											
176.3			32											
173.5			33											
170.7			34											
167.9			35											
165.1			36											
162.3			37											
159.5			38											
156.7			39											
153.9			40											
151.1			41											
148.3			42											
145.5			43											
142.7			44											
139.9			45											
137.1			46											
134.3			47											
131.5			48											
128.7			49											
125.9			50											
123.1			51											
120.3			52											
117.5			53											
114.7			54											
111.9			55											
109.1			56											
106.3			57											
103.5			58											
100.7			59											
97.9			60											
95.1			61											
92.3			62											
89.5			63											
86.7			64											
83.9			65											
81.1			66											
78.3			67											
75.5			68											
72.7			69											
69.9			70											
67.1			71											
64.3			72											
61.5			73											
58.7			74											
55.9			75											
53.1			76											
50.3			77											
47.5			78											
44.7			79											
41.9			80											
39.1			81											
36.3			82											
33.5			83											
30.7			84											
27.9			85											
25.1			86											
22.3			87											
19.5			88											
16.7			89											
13.9			90											
11.1			91											
8.3			92											
5.5			93											
2.7			94											
0.0			95											
256.0	END OF BOREHOLE: Notes: 1) Water encountered at 2.5m during drilling.		17	SS	50/130mm									

GROUNDWATER ELEVATIONS
Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity
○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27

PROJECT: Geotechnical Investigation
CLIENT: Times Group Corporation
PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON
DATUM: Geodetic
BH LOCATION: See Drawing 1 N 4869103.6 E 637709.7

DRILLING DATA
Method: Hollow Stem Auger/Mud Rotary
Diameter: 200mm
Date: Nov-04-2024
REF. NO.: 19-043-103
ENCL NO.: 12

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT		POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		W _p	W			
256.3								20 40 60 80 100						GR SA SI CL
256.0	TOPSOIL: 250mm		1	SS	8		256							Switched to Mud Rotary
255.5	FILL: silty clay, trace rootlets, trace gravel, trace organics, dark brown to brown, moist, stiff		2	SS	11		255							
255.0	CLAYEY SILT TILL: sandy, trace gravel, brown, moist, stiff to hard sandy silt pockets at 1.5m		3	SS	13		254							
254.5			4	SS	19		253							
254.0			5	SS	33		252							
253.5	SILT: trace sand, trace gravel, brown, very moist, dense		6	SS	40		251							
253.0	SILTY SAND: trace clay, brown, wet, dense		7	SS	47		250							
252.5	silt pockets at 4.6m		8	SS	41		249							
252.0			9	SS	50/150mm		248							
251.5	CLAYEY SILT TILL: some sand to sandy, trace gravel, occasional cobble, grey, moist, very stiff to hard		10	SS	50/130mm		247							
251.0			11	SS	74		246							
250.5	wet silt layer, very stiff at 8.4m		12	SS	22		245							
250.0			13	SS	39		244							
249.5	SILT: trace sand, trace clay, grey, moist, dense		14	SS	50/150mm		243							
249.0			15	SS	50/130mm		242							
248.5	SANDY SILT TO SILTY SAND TILL: trace to some clay, trace gravel, occasional cobble, grey, moist to wet, very dense		16	SS	50/130mm		241							
248.0			17	SS	50/150mm		240							
247.5	CLAYEY SILT TILL: sandy, trace gravel, occasional cobble, grey, moist, hard													
247.0	END OF BOREHOLE: Notes: 1) Water encountered at 2.7m during drilling.													

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27

PROJECT: Geotechnical Investigation
CLIENT: Times Group Corporation
PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON
DATUM: Geodetic
BH LOCATION: See Drawing 1 N 4869069.4 E 637689.9

DRILLING DATA
Method: Hollow Stem Auger/Mud Rotary
Diameter: 200mm
Date: Oct-23-2024
REF. NO.: 19-043-103
ENCL NO.: 13

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT			POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)
(m)	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			20 40 60 80 100	20 40 60 80 100	W _p	W	W _L			
256.6															GR SA SI CL
256.4	TOPSOIL: 250mm		1	SS	11		256								
0.3	FILL: silty clay, trace rootlets, trace gravel, trace organics, dark brown to brown, moist, stiff														
255.6			2	SS	11		255								
1.0	CLAYEY SILT: trace sand, trace gravel, brown, moist, stiff														
255.1			3	SS	44		254								
1.5	SILTY SAND: trace clay, some gravel, brown, moist, dense														
254.3			4	SS	16		253								
2.3	CLAYEY SILT TILL: sandy, trace gravel, brown, moist, very stiff														
			5	SS	20		252								
252.1															
4.5	SANDY SILT TO SAND: trace clay, brown, wet, dense		6	SS	35		251								
250.6							250								
6.0	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, very stiff		7	SS	28		249								
249.1															
7.5	CLAYEY SILT: trace sand, grey, moist, very stiff to hard		8	SS	49		248								
	silt layer at 9.1m		9	SS	23		247								
246.1							246								
10.5	SANDY SILT TILL: trace to some clay, trace gravel, occasional cobble, grey, moist, very dense		10	SS	50/130mm		245								
244.6															
12.0	SANDY SILT: trace clay, grey, wet, very dense		11	SS	50/130mm		244								
243.1															
13.5	SANDY SILT TO SILTY SAND TILL: trace clay, trace gravel, occasional cobble, grey, moist to very moist, very dense		12	SS	50/100mm		243								
							242								
			13	SS	50/130mm		241								
							240								

Switched to Mud Rotary

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103GEO.GPJ DS.GDT 24-11-27

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

REF. NO.: 19-043-103





Date: Oct-23-2024

ENCL NO.: 13

BH LOCATION: See Drawing 1 N 4869069.4 E 637689.9

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%) GR SA SI CL		
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)								WATER CONTENT (%)	
								○ UNCONFINED ● QUICK TRIAXIAL	+ FIELD VANE & Sensitivity × LAB VANE								
238.3	SANDY SILT TO SILTY SAND TILL: trace clay, trace gravel, occasional cobble, grey, moist to very moist, very dense(Continued)		14	SS	50/ 30mm	239											
18.3	CLAYEY SILT TILL: sandy, trace gravel, grey, moist, hard		15	SS	50/ 30mm	238									9 41 37 13		
			16	SS	50/ 30mm	237											
			17	SS	50/ 30mm	235											
233.6	END OF BOREHOLE: Notes: 1) Water encountered at 4.6m during drilling.		18	SS	50/ 100mm	234											

GROUNDWATER ELEVATIONS

	1st	2nd	3rd	4th
Measurement				

GRAPH
NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ **ε**=3% Strain at Failure



PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869140.7 E 637861

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Feb-26-2025

REF. NO.: 19-043-103

ENCL NO.: 14

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	POCKET PEN. (C _u) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)			
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m		SHEAR STRENGTH (kPa)										WATER CONTENT (%)		
							○ UNCONFINED + FIELD VANE & Sensitivity ● QUICK TRIAXIAL × LAB VANE										W _P W W _L		
254.3							20	40	60	80	100	10	20	30		GR SA SI CL			
254.0	0.2	TOPSOIL: 200mm	1	SS	3		W. L. 254.5 m						○						
253.9		FILL: clayey silt, trace organics, trace rootlets, trace sand to some sand, brown, moist, soft to stiff	2	SS	4		Mar 24, 2025						○						
252.6	1.7	CLAYEY SILT TO SILTY CLAY TILL: sandy, trace gravel, brown to grey, moist, stiff to hard	3	SS	11		W. L. 253.5 m						○						
		silty sand layer at 3.1m	4	SS	24		Mar 07, 2025						○						
			5	SS	44								○			Switched to Mud Rotary			
		grey below 4.6m	6	SS	31								○						
			7	SS	36								○						
			8	SS	18								○						
		stiff at 9.1m	9	SS	9								○			4 23 48 25			
243.6	10.7	SILTY SAND TO SANDY SILT TILL: trace to some clay, trace to some gravel, cobble/boulder, grey, very moist to wet, compact to very dense	10	SS	28								○						
		clayey silt till layers below 12.5m	11	SS	50/ 75mm								○						
			12	SS	21								○			9 48 35 8			
239.3	15.0	SILTY SAND: trace clay, trace gravel, grey, very moist to wet, very dense (till - like)	13	SS	45								○						
			14	SS	65								○			8 61 27 4			
236.3	18.0	SILTY SAND TO SANDY SILT TILL: trace clay, trace to some gravel, cobble/boulder, grey, very moist to wet, very dense	15	SS	50/ 100mm								○						
			16	SS	50/ 75mm								○			3 32 57 8			
233.0	21.3		17	SS	50/ 75mm								○						

Continued Next Page

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH
NOTES+ 3 × 3: Numbers refer
to Sensitivity

○ = 3% Strain at Failure

PROJECT: Geotechnical Investigation

CLIENT: Times Group Corporation

PROJECT LOCATION: 5061 Stouffville Road, Whitchurch-Stouffville, ON

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4869140.7 E 637861

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Feb-26-2025

REF. NO.: 19-043-103

ENCL NO.: 14

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT	NATURAL MOISTURE CONTENT	LIQUID LIMIT	POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (kN/m ³)	REMARKS AND GRAIN SIZE DISTRIBUTION (%)			
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	"N" BLOWS 0.3 m			SHEAR STRENGTH (kPa)		W _p	W	W _L			GR	SA	SI	CL
254.3	TOPSOIL: 200mm		1	SS	3		254.3	20	100									
254.0	FILL: clayey silt, trace organics, trace rootlets, trace sand to some sand, brown, moist, soft to stiff		2	SS	4		254.1	20	100									
252.6	CLAYEY SILT TO SILTY CLAY TILL: sandy, trace gravel, brown to grey, moist, stiff to hard		3	SS	11		253	20	100									
251.7			4	SS	24		252	20	100									
	silty sand layer at 3.1m		5	SS	44		251	20	100									
			6	SS	31		250	20	100									
	grey below 4.6m		7	SS	36		249	20	100									
			8	SS	18		248	20	100									
			9	SS	9		247	20	100									
	stiff at 9.1m		10	SS			246	20	100									
243.6	SILTY SAND TO SANDY SILT TILL: trace to some clay, trace to some gravel, cobble/boulder, grey, very moist to wet, compact to very dense		11	SS	28		245	20	100						4	23	48	25
243.6			12	SS			244	20	100									
243.6	clayey silt till layers below 12.5m		13	SS	50/ 75mm		243	20	100									
243.6			14	SS	21		242	20	100									
243.6			15	SS			241	20	100									
239.3	SILTY SAND: trace clay, trace gravel, grey, very moist to wet, very dense (till - like)		16	SS	45		240	20	100						9	48	35	8
239.3			17	SS	65		239	20	100									
239.3			18	SS			238	20	100									
236.3	SILTY SAND TO SANDY SILT TILL: trace clay, trace to some gravel, cobble/boulder, grey, very moist to wet, very dense		19	SS	50/ 100mm		237	20	100						8	61	27	4
236.3			20	SS			236	20	100									
236.3			21	SS	50/ 75mm		235	20	100									
236.3			22	SS			234	20	100									
233.0			23	SS	50/ 75mm		233	20	100						3	32	57	8
233.0			24	SS			232	20	100									
233.0			25	SS			231	20	100									
233.0			26	SS			230	20	100									
233.0			27	SS			229	20	100									
233.0			28	SS			228	20	100									
233.0			29	SS			227	20	100									
233.0			30	SS			226	20	100									
233.0			31	SS			225	20	100									
233.0			32	SS			224	20	100									
233.0			33	SS			223	20	100									
233.0			34	SS			222	20	100									
233.0			35	SS			221	20	100									
233.0			36	SS			220	20	100									
233.0			37	SS			219	20	100									
233.0			38	SS			218	20	100									
233.0			39	SS			217	20	100									
233.0			40	SS			216	20	100									
233.0			41	SS			215	20	100									
233.0			42	SS			214	20	100									
233.0			43	SS			213	20	100									
233.0			44	SS			212	20	100									
233.0			45	SS			211	20	100									
233.0			46	SS			210	20	100									
233.0			47	SS			209	20	100									
233.0			48	SS			208	20	100									
233.0			49	SS			207	20	100									
233.0			50	SS			206	20	100									
233.0			51	SS			205	20	100									
233.0			52	SS			204	20	100									
233.0			53	SS			203	20	100									
233.0			54	SS			202	20	100									
233.0			55	SS			201	20	100									
233.0			56	SS			200	20	100									
233.0			57	SS			199	20	100									
233.0			58	SS			198	20	100									
233.0			59	SS			197	20	100									
233.0			60	SS			196	20	100									
233.0			61	SS			195	20	100									
233.0			62	SS			194	20	100									
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233.0			64	SS			192	20	100									
233.0			65	SS			191	20	100									
233.0			66	SS			190	20	100									
233.0			67	SS			189	20	100									
233.0			68	SS			188	20	100									
233.0			69	SS			187	20	100									
233.0			70	SS			186	20	100									
233.0			71	SS			185	20	100									
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233.0			73	SS			183	20	100									
233.0			74	SS			182	20	100									
233.0			75	SS			181	20	100									
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233.0			77	SS			179	20	100									
233.0			78	SS			178	20	100									
233.0			79	SS			177	20	100									
233.0			80	SS			176	20	100									
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233.0			82	SS			174	20	100									
233.0			83	SS			173	20	100									
233.0			84	SS			172	20	100									
233.0			85	SS			171	20	100									
233.0			86	SS			170	20	100									
233.0			87	SS			169	20	100									
233.0			88	SS			168	20	100									
233.0			89	SS			167	20	100									
233.0			90	SS			166	20	100									
233.0			91	SS			165	20	100									
233.0			92	SS			164	20	100									
233.0			93	SS			163	20	100									
233.0			94	SS			162	20	100									
233.0			95	SS			161	20	100									
233.0			96	SS			160	20	100									
233.0			97	SS			159	20	100									
233.0			98	SS			158	20	100									
233.0			99	SS			157	20	100									
233.0			100	SS			156	20	100									

Continued Next Page

GROUNDWATER ELEVATIONS
1st 2nd 3rd 4th
Measurement

GRAPH
NOTES

+ 3 × 3: Numbers refer to Sensitivity
○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 19-043-103 GEO.GPJ DS GDT 25-4-4

DRILLING DATA

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

REF. NO.: 19-043-103





Date: Feb-26-2025

ENCL NO.: 14

BH LOCATION: See Drawing 1 N 4869140.7 E 637861

[illegible]

GROUNDWATER ELEVATIONS

	1st	2nd	3rd	4th
Measurement				

GRAPH
NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ **$\epsilon=3\%$** Strain at Failure



Appendix B



Slug Test Analysis Report

Project: 4721-5061 Stouffville Road

Number: 19-043-100

Client: Times Group

Location: Stouffville Road

Slug Test: MW19-5

Test Well: MW19-5

Test Conducted by: PP

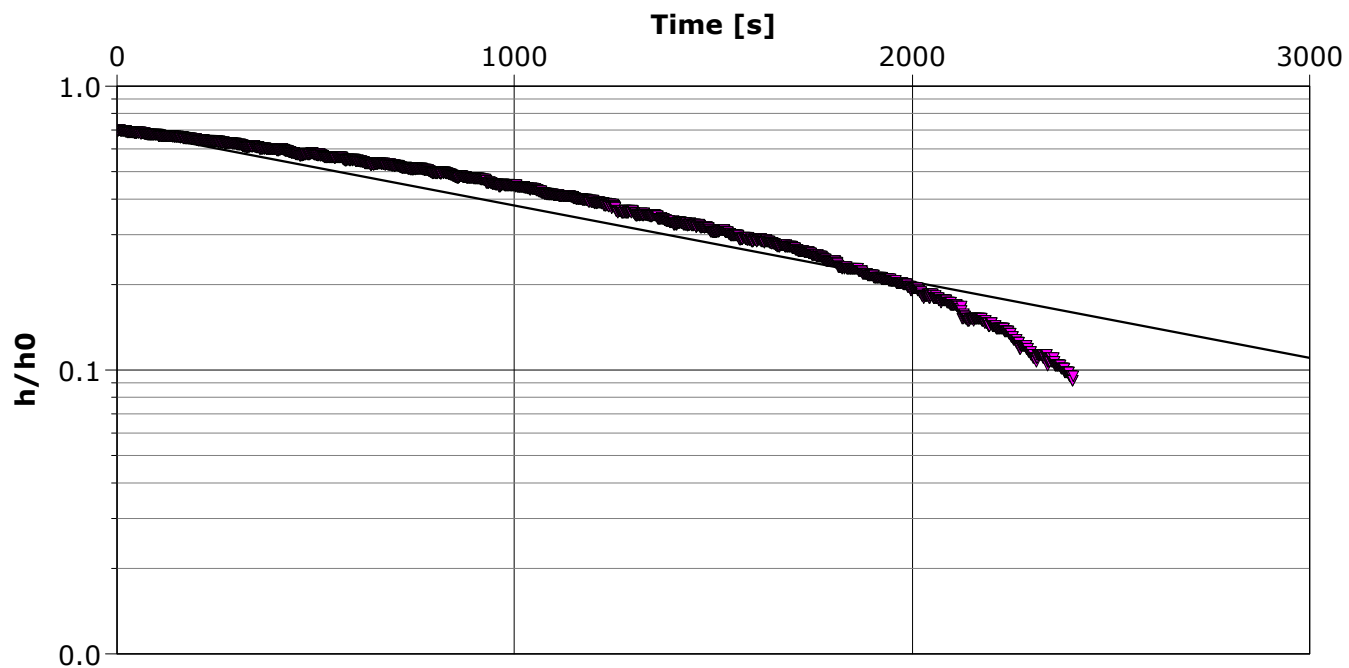
Test Date: 2019-05-24

Analysis Performed by: DG

MW19-5

Analysis Date: 2019-05-27

Aquifer Thickness:



▼ MW19-5

Calculation using Hvorslev

Observation Well

Hydraulic Conductivity
[m/s]

MW19-5

3.10×10^{-7}



Slug Test Analysis Report

Project: 4721-5061 Stouffville Road

Number: 19-043-101

Client: Times Group

Location: Whitchurch-Stouffville

Slug Test: BH21-1

Test Well: BH21-1

Test Conducted by: MP

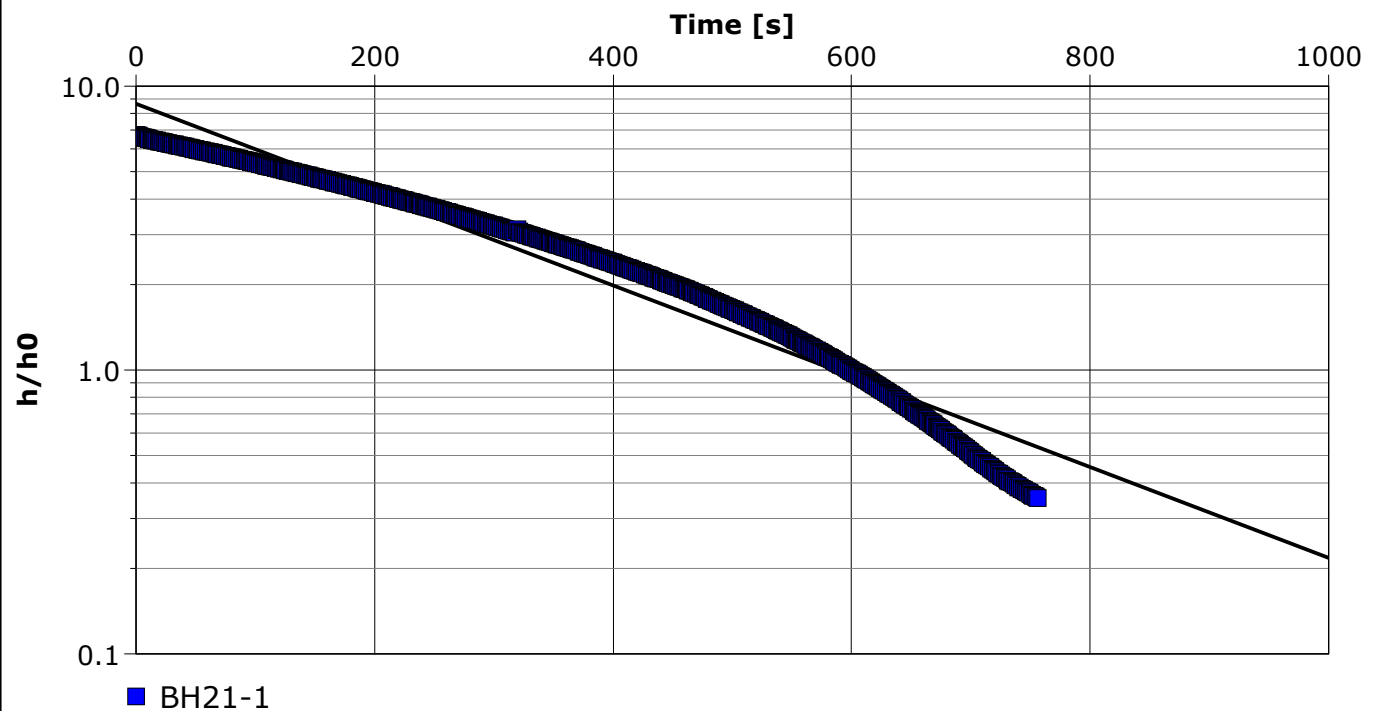
Test Date: 2021-02-25

Analysis Performed by: DG

BH21-1

Analysis Date: 2019-05-27

Aquifer Thickness: 15.80 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH21-1

1.61×10^{-6}



Slug Test Analysis Report

Project: 4721-5061 Stouffville Road

Number: 19-043-101

Client: Times Group

Location: Whitchurch-Stouffville

Slug Test: BH21-3

Test Well: BH21-3

Test Conducted by: MP

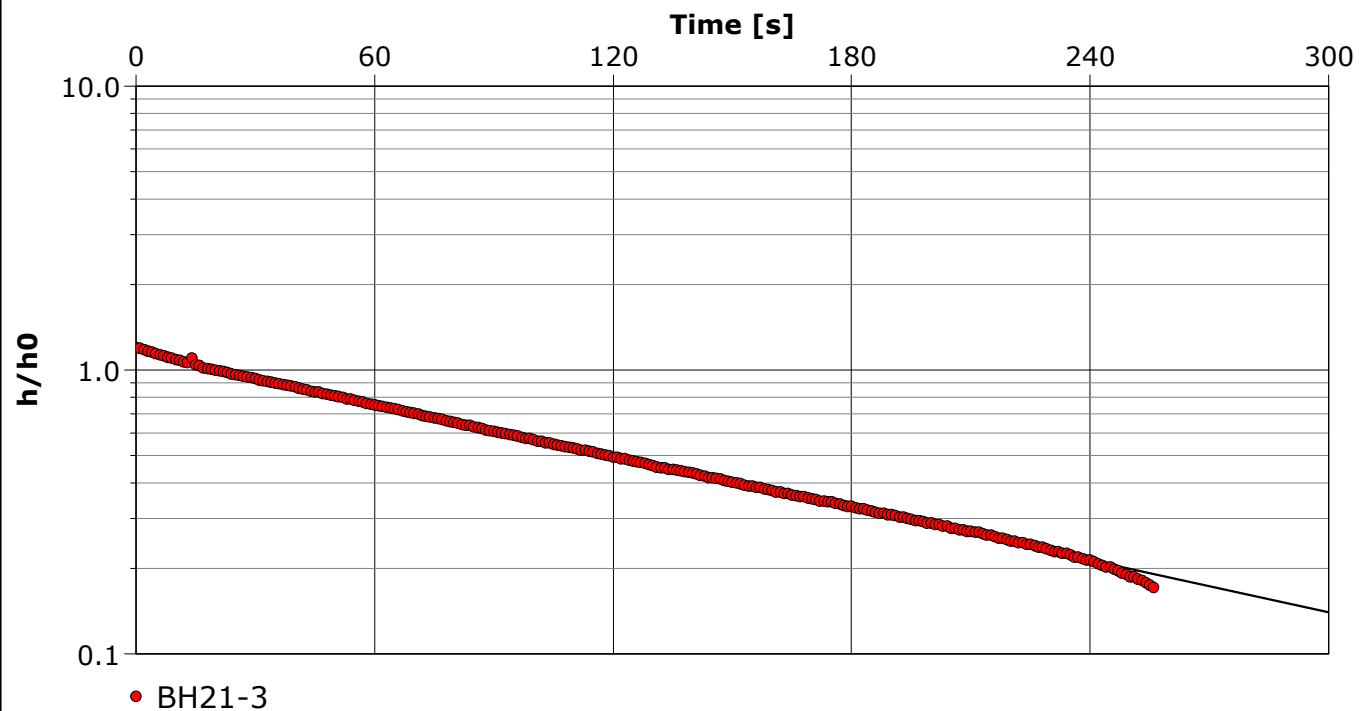
Test Date: 2021-02-25

Analysis Performed by: DG

BH21-3

Analysis Date: 2019-05-27

Aquifer Thickness: 16.30 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH21-3

4.89×10^{-6}



Slug Test Analysis Report

Project: 4721-5061 Stouffville Road

Number: 19-043-101

Client: Times Group

Location: Whitchurch-Stouffville

Slug Test: BH21-4

Test Well: BH21-4

Test Conducted by: MP

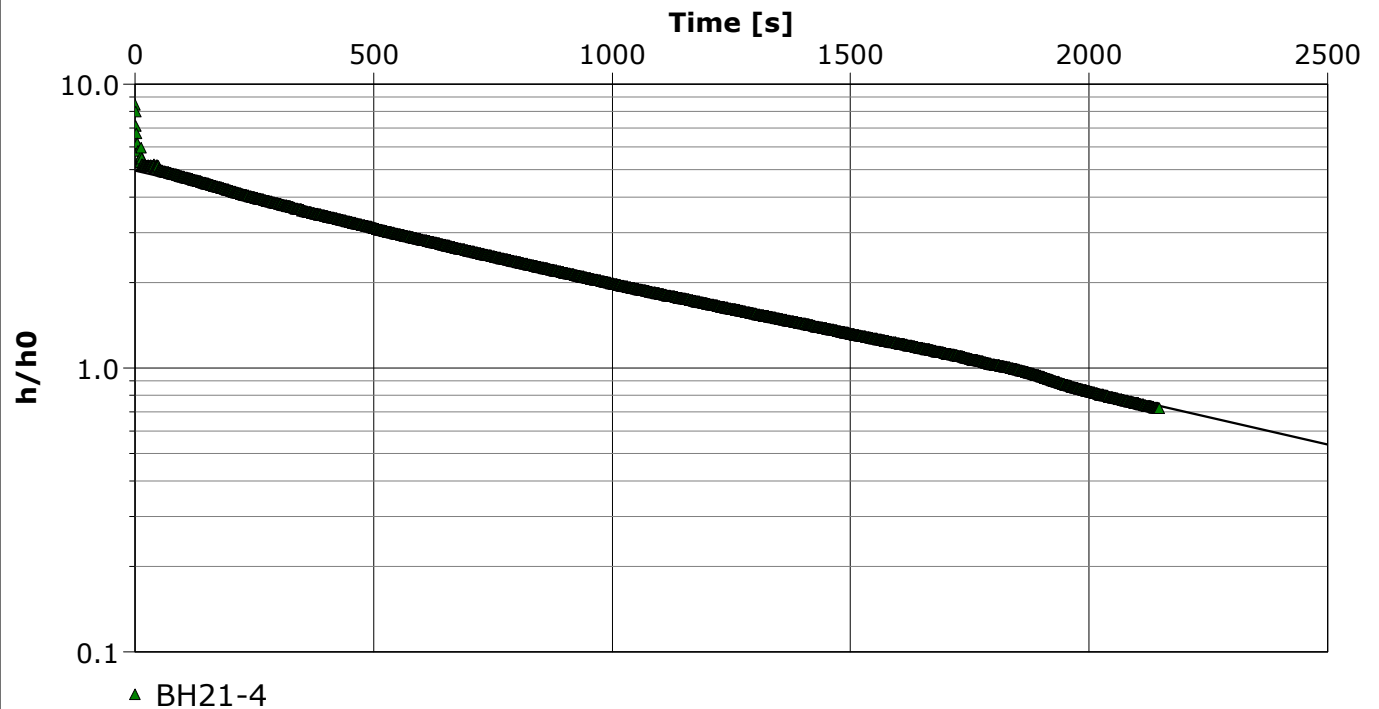
Test Date: 2021-02-25

Analysis Performed by: DG

BH21-4

Analysis Date: 2019-05-27

Aquifer Thickness: 15.30 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH21-4

6.83×10^{-7}



Slug Test Analysis Report

Project: 5061 Stouffville Road

Number: 19-043-103

Client: Times Group Corporation

Location: Whitchurch-Stouffville, ON

Slug Test: BH24-1

Test Well: BH24-1

Test Conducted by: CL

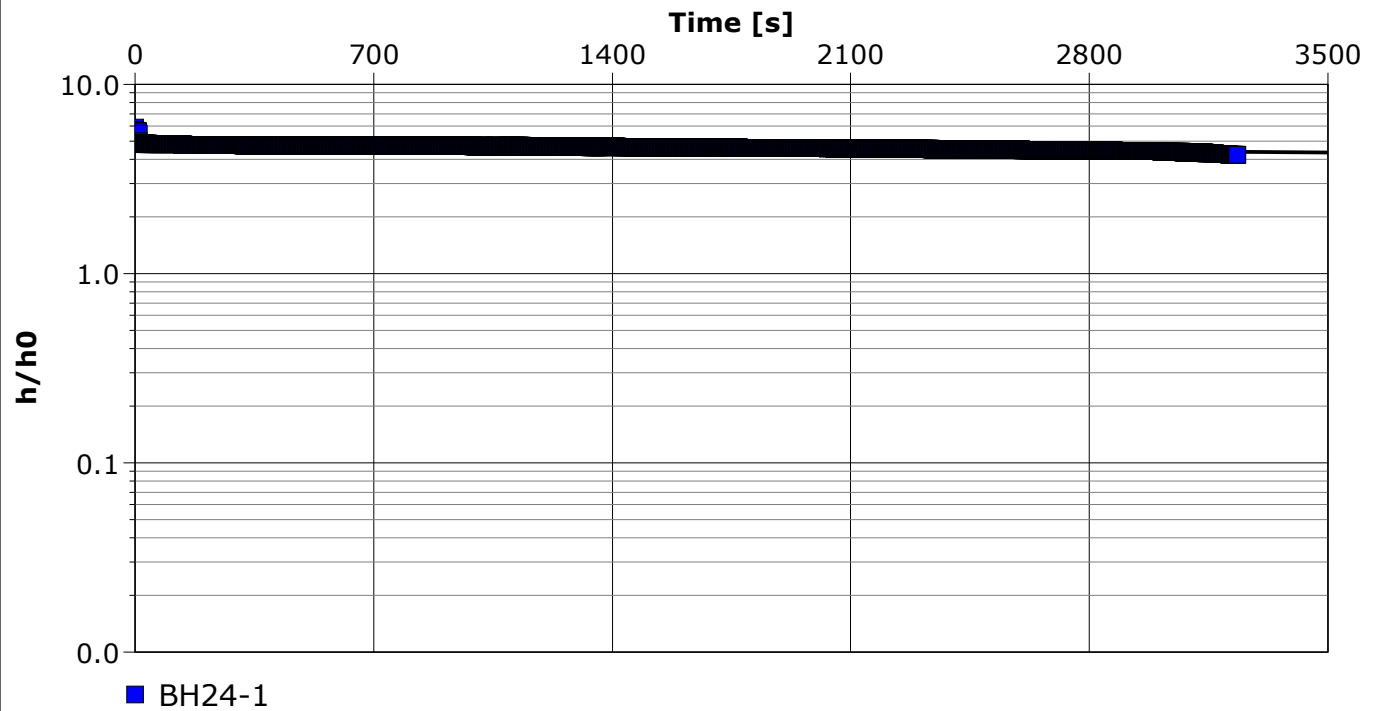
Test Date: 11/13/2024

Analysis Performed by: DS

BH24-1

Analysis Date: 11/8/2024

Aquifer Thickness: 23.00 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH24-1

1.09×10^{-8}



Slug Test Analysis Report

Project: 5061 Stouffville Road

Number: 19-043-103

Client: Times Group Corporation

Location: Whitchurch-Stouffville, ON

Slug Test: BH24-4

Test Well: BH24-4

Test Conducted by: CL

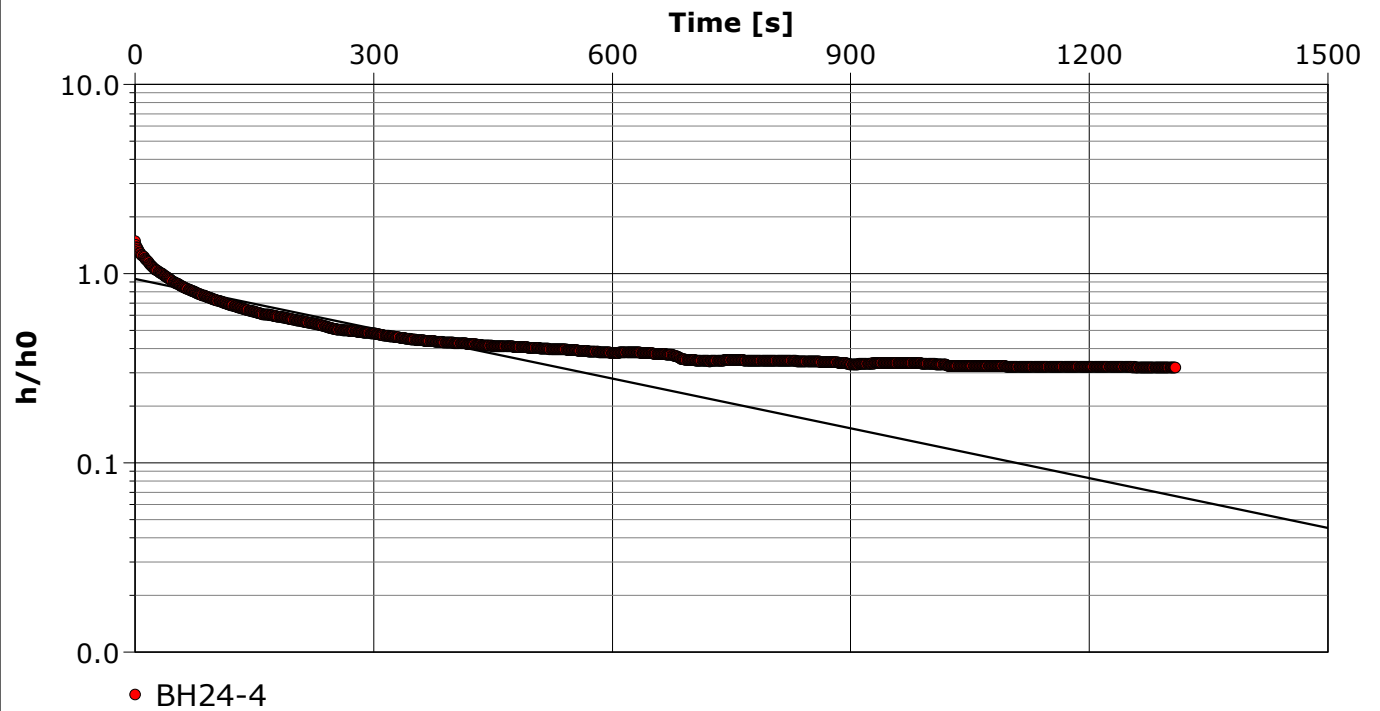
Test Date: 11/13/2024

Analysis Performed by: DS

BH24-4

Analysis Date: 11/8/2024

Aquifer Thickness: 9.00 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH24-4

7.52×10^{-7}



Slug Test Analysis Report

Project: 5061 Stouffville Road

Number: 19-043-103

Client: Times Group Corporation

Location: Whitchurch-Stouffville, ON

Slug Test: BH24-5

Test Well: BH24-5

Test Conducted by: CL

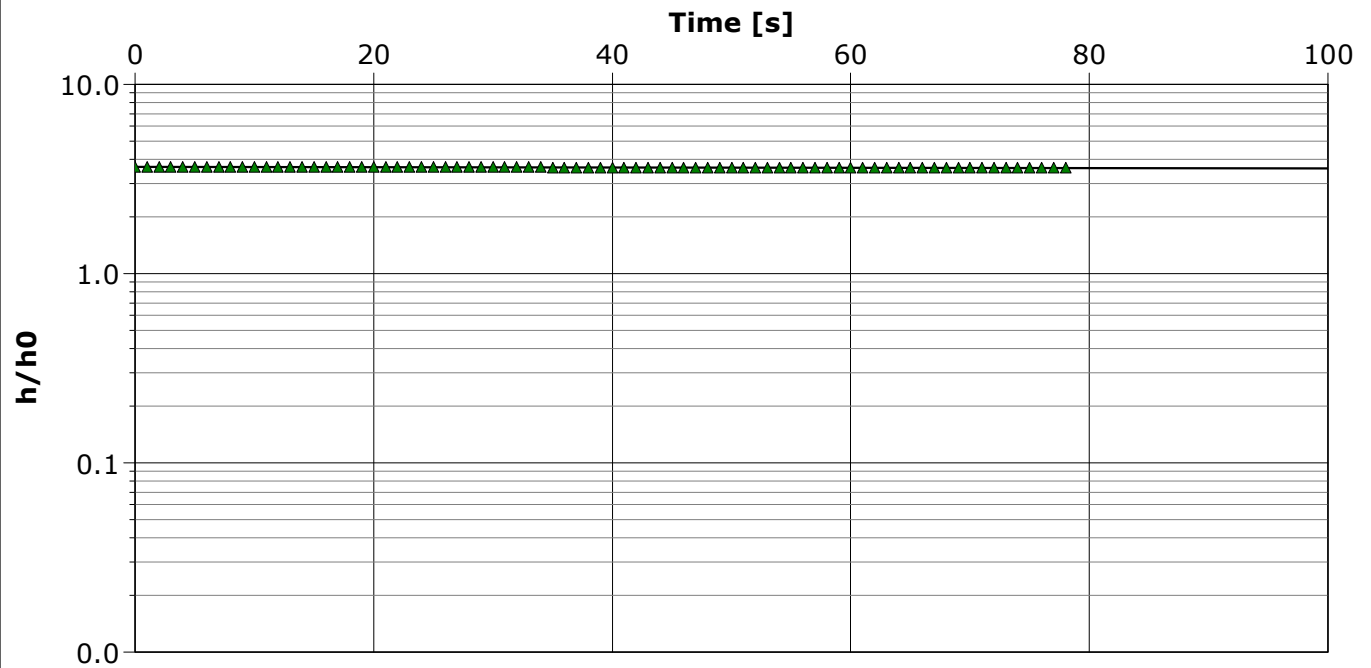
Test Date: 11/13/2024

Analysis Performed by: DS

BH24-5

Analysis Date: 11/22/2024

Aquifer Thickness: 10.50 m



▲ BH24-5

Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH24-5

7.14×10^{-8}



Slug Test Analysis Report

Project: 5061 Stouffville Road

Number: 19-043-103

Client: Times Group Corporation

Location: Whitchurch-Stouffville, ON

Slug Test: BH24-8

Test Well: BH24-8

Test Conducted by: CL

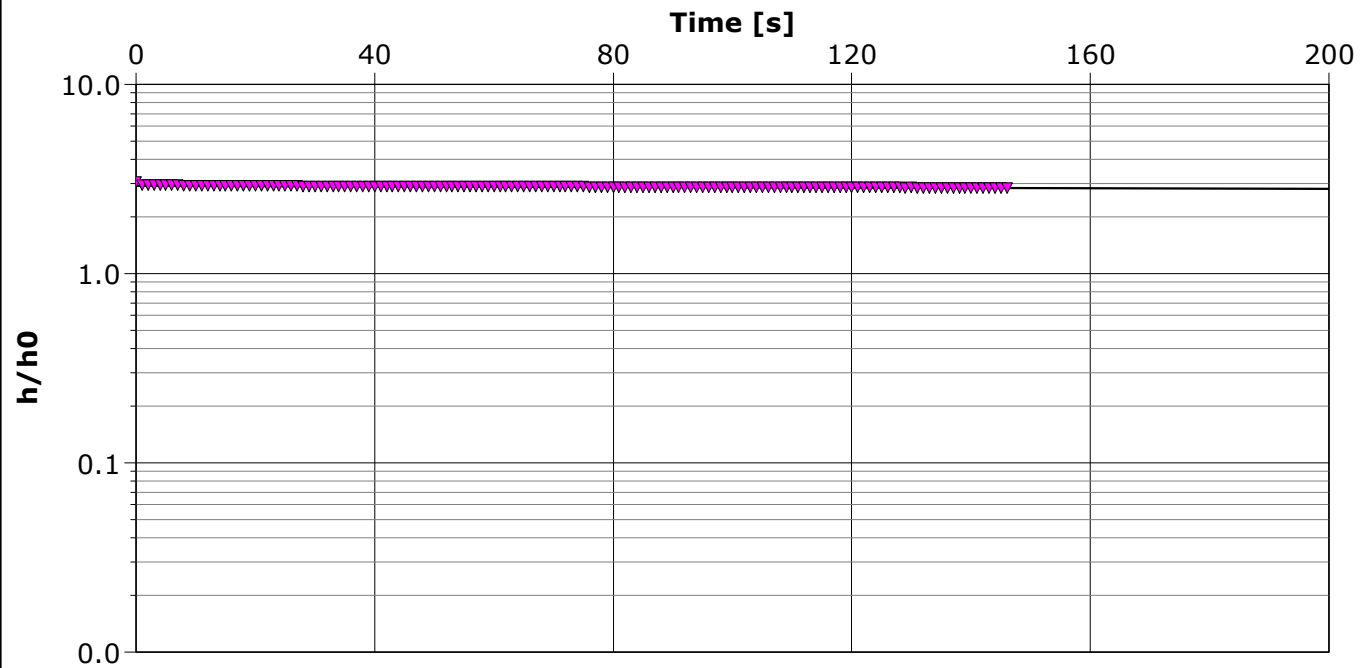
Test Date: 11/13/2024

Analysis Performed by: DS

BH24-8

Analysis Date: 11/22/2024

Aquifer Thickness: 7.50 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH24-8

7.51×10^{-8}



Slug Test Analysis Report

Project: 5061 Stouffville Road

Number: 19-043-103

Client: Times Group Corporation

Location: Whitchurch-Stouffville, ON

Slug Test: BH24-9

Test Well: BH24-9

Test Conducted by: DS

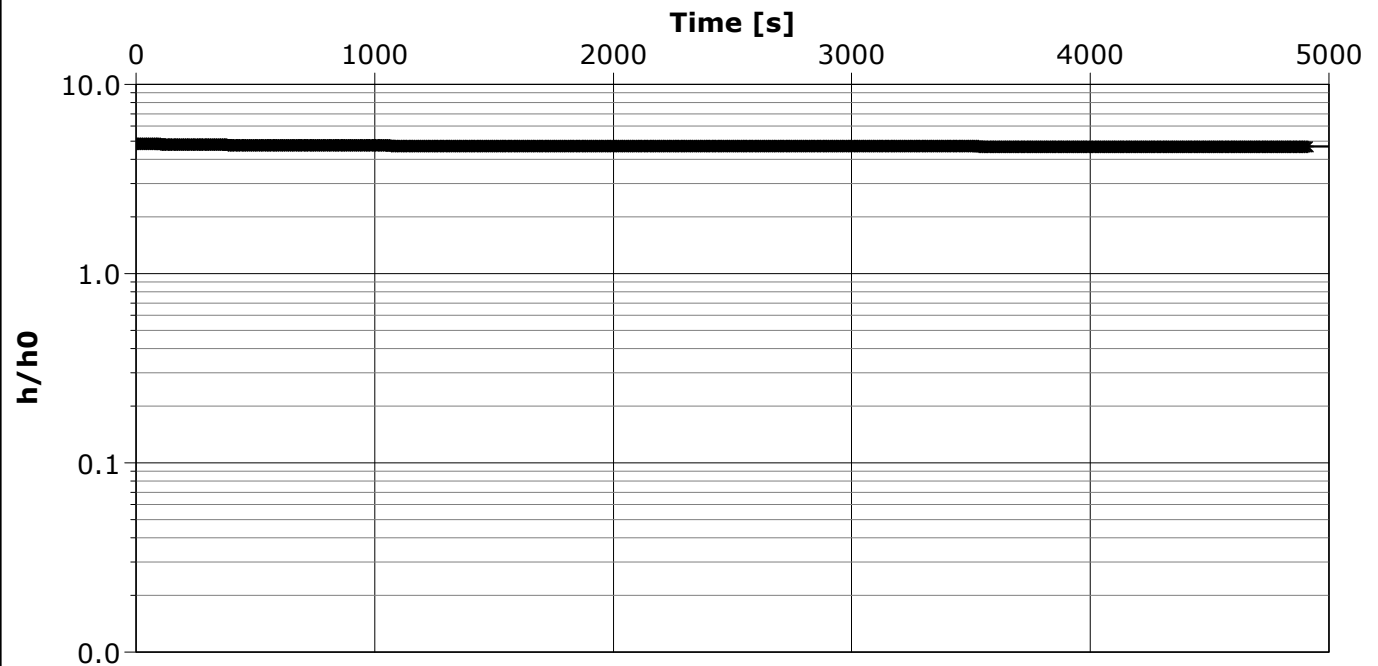
Test Date: 11/13/2024

Analysis Performed by: DS

BH24-9

Analysis Date: 11/22/2024

Aquifer Thickness: 9.00 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH24-9

1.91×10^{-9}



Slug Test Analysis Report

Project: 5061 Stouffville Road

Number: 19-043-103

Client: Times Group Corporation

Location: Whitchurch-Stouffville, ON

Slug Test: BH25-1

Test Well: BH25-1

Test Conducted by: KK

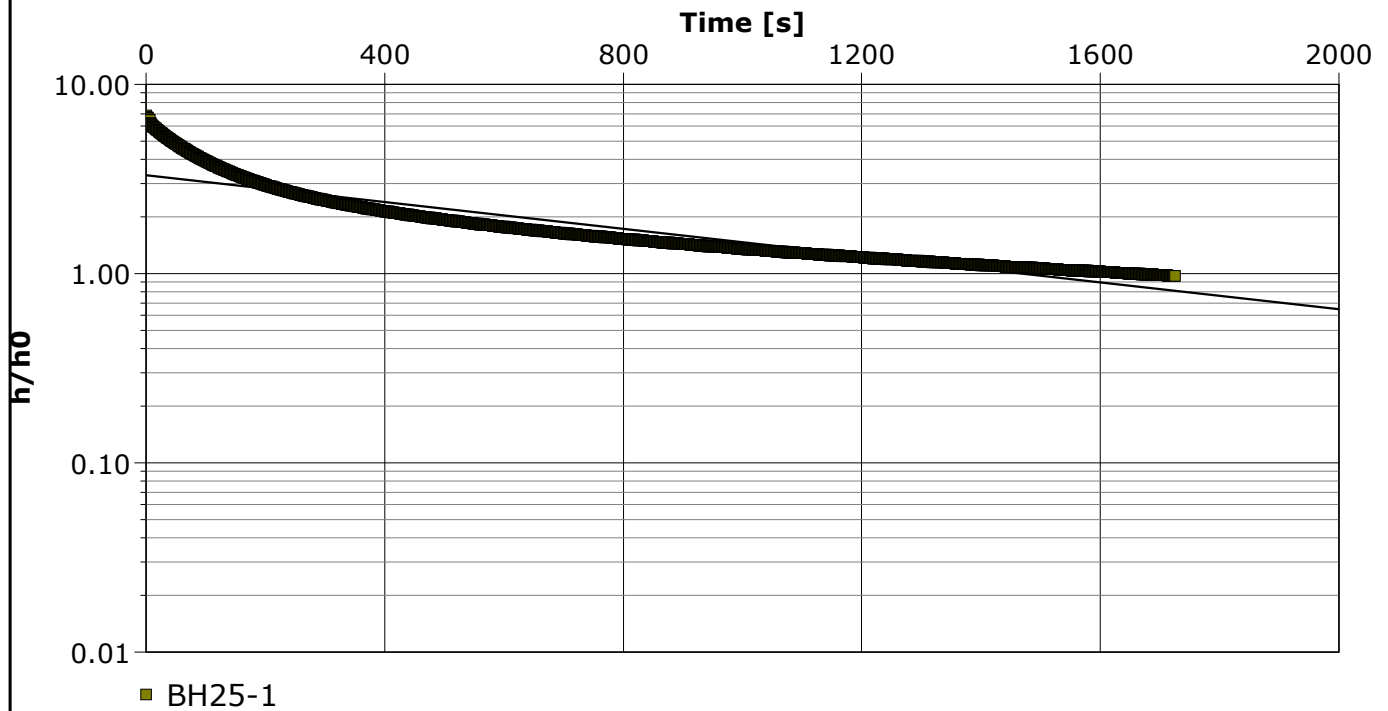
Test Date: 3/24/2025

Analysis Performed by: DS

BH25-1

Analysis Date: 3/28/2025

Aquifer Thickness: 40.00 m



Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[m/s]

BH25-1

3.24×10^{-7}



Appendix C



FINAL REPORT

CA40064-OCT24 R1

19-043-101, 4721-5061 Stouffville Rd.

Prepared for

DS Consultants

First Page

CLIENT DETAILS

Client DS Consultants

Address 6221 Highway 7 Unit 6
Vaughan, Ontario
L4H 0K8, Canada

Contact Don Hsu

Telephone 905-264-9393

Facsimile 905-264-2685

Email don.hsu@dsconsultants.ca

Project 19-043-101, 4721-5061 Stouffville Rd.

Order Number

Samples Ground Water (1)

LABORATORY DETAILS

Project Specialist Maarit Wolfe, Hon.B.Sc

Laboratory SGS Canada Inc.

Address 185 Concession St., Lakefield ON, K0L 2H0

Telephone 705-652-2000

Facsimile 705-652-6365

Email Maarit.Wolfe@sgs.com

SGS Reference CA40064-OCT24

Received 10/07/2024

Approved 10/15/2024

Report Number CA40064-OCT24 R1

Date Reported 10/15/2024

COMMENTS

RL - SGS Reporting Limit

Nonylphenol Ethoxylates is the sum of nonylphenol monoethoxylate and nonylphenol diethoxylate.

Temperature of Sample upon Receipt: 9 degrees C

Cooling Agent Present: yes

Custody Seal Present: yes

Chain of Custody Number: 035639

SIGNATORIES

Maarit Wolfe, Hon.B.Sc





TABLE OF CONTENTS

First Page..... 1

Index..... 2

Results..... 3-6

Exceedance Summary..... 7

QC Summary..... 8-16

Legend..... 17

Annexes..... 18



FINAL REPORT

CA40064-OCT24 R1

Client: DS Consultants

Project: 19-043-101, 4721-5061 Stouffville Rd.

Project Manager: Don Hsu

Samplers: Don Hsu

MATRIX: WATER

Sample Number 8

Sample Name BH 19-5

Sample Matrix Ground Water

Sample Date 07/10/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102

L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
-----------	-------	----	----	----	--------

General Chemistry

Biochemical Oxygen Demand (BOD5)	mg/L	2	300	15	< 4 †
Total Suspended Solids	mg/L	2	350	15	9
Total Kjeldahl Nitrogen	as N mg/L	0.5	100	1	< 0.5

Metals and Inorganics

Sulphate	mg/L	2	1500		5
Cyanide (total)	mg/L	0.01	2	0.02	< 0.01
Fluoride	mg/L	0.06	10		0.16
Aluminum (total)	mg/L	0.001	50		0.048
Antimony (total)	mg/L	0.0009	5		< 0.0009
Arsenic (total)	mg/L	0.0002	1	0.02	0.0014
Cadmium (total)	mg/L	0.000003	0.7	0.008	< 0.000003
Chromium (total)	mg/L	0.00008	2	0.08	0.00022
Cobalt (total)	mg/L	0.000004	5		0.000042
Copper (total)	mg/L	0.001	3	0.05	< 0.001
Lead (total)	mg/L	0.00009	1	0.12	0.00010
Manganese (total)	mg/L	0.00001	5	0.15	0.0131
Molybdenum (total)	mg/L	0.0004	5		0.0010
Nickel (total)	mg/L	0.0001	2	0.08	< 0.0001
Phosphorus (total)	mg/L	0.003	10	0.4	0.019
Selenium (total)	mg/L	0.00004	1	0.02	< 0.00004
Silver (total)	mg/L	0.00005	5	0.12	< 0.00005
Tin (total)	mg/L	0.00006	5		0.00039



FINAL REPORT

CA40064-OCT24 R1

Client: DS Consultants
Project: 19-043-101, 4721-5061 Stouffville Rd.
Project Manager: Don Hsu
Samplers: Don Hsu

MATRIX: WATER

Sample Number 8
Sample Name BH 19-5
Sample Matrix Ground Water
Sample Date 07/10/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102
L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
Metals and Inorganics (continued)					
Titanium (total)	mg/L	0.0001	5		0.0025
Zinc (total)	mg/L	0.002	2	0.04	< 0.002
Nonylphenol and Ethoxylates					
Nonylphenol	mg/L	0.001	0.02		< 0.001
Nonylphenol Ethoxylates	mg/L	0.01	0.2		< 0.01
Nonylphenol diethoxylate	mg/L	0.01			< 0.01
Nonylphenol monoethoxylate	mg/L	0.01			< 0.01
Oil and Grease					
Oil & Grease (total)	mg/L	2			< 2
Oil & Grease (animal/vegetable)	mg/L	4	150		< 4
Oil & Grease (mineral/synthetic)	mg/L	4	15		< 4
Other (ORP)					
pH	No unit	0.05	10.5	9	8.01
Mercury (total)	mg/L	0.00001	0.01	0.0004	< 0.00001



FINAL REPORT

CA40064-OCT24 R1

Client: DS Consultants
Project: 19-043-101, 4721-5061 Stouffville Rd.
Project Manager: Don Hsu
Samplers: Don Hsu

MATRIX: WATER

Sample Number 8
Sample Name BH 19-5
Sample Matrix Ground Water
Sample Date 07/10/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102
L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
PCBs					
Polychlorinated Biphenyls (PCBs) - Total	mg/L	0.0001	0.001	0.0004	< 0.0001
Phenols					
4AAP-Phenolics	mg/L	0.002	1	0.008	< 0.002
SVOCs					
di-n-Butyl Phthalate	mg/L	0.002	0.08	0.015	< 0.002
Bis(2-ethylhexyl)phthalate	mg/L	0.002	0.012	0.0088	< 0.002
VOCs					
Chloroform	mg/L	0.0005	0.04	0.002	< 0.0005
1,2-Dichlorobenzene	mg/L	0.0005	0.05	0.0056	< 0.0005
1,4-Dichlorobenzene	mg/L	0.0005	0.08	0.0068	< 0.0005
cis-1,2-Dichloroethylene	mg/L	0.0005	4	0.0056	< 0.0005
trans-1,3-Dichloropropene	mg/L	0.0005	0.14	0.0056	< 0.0005
Methylene Chloride	mg/L	0.0005	2	0.0052	< 0.0005
1,1,2,2-Tetrachloroethane	mg/L	0.0005	1.4	0.017	< 0.0005
Tetrachloroethylene (perchloroethylene)	mg/L	0.0005	1	0.0044	< 0.0005
Trichloroethylene	mg/L	0.0005	0.4	0.008	< 0.0005
Methyl ethyl ketone	mg/L	0.02	8		< 0.02
Styrene	mg/L	0.0005	0.2		< 0.0005



FINAL REPORT

CA40064-OCT24 R1

Client: DS Consultants
Project: 19-043-101, 4721-5061 Stouffville Rd.
Project Manager: Don Hsu
Samplers: Don Hsu

MATRIX: WATER

Sample Number 8
Sample Name BH 19-5
Sample Matrix Ground Water
Sample Date 07/10/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102
L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
VOCs - BTEX					
Benzene	mg/L	0.0005	0.01	0.002	< 0.0005
Ethylbenzene	mg/L	0.0005	0.16	0.002	< 0.0005
Toluene	mg/L	0.0005	0.27	0.002	< 0.0005
Xylene (total)	mg/L	0.0005	1.4	0.0044	< 0.0005
m-p-xylene	mg/L	0.0005			< 0.0005
o-xylene	mg/L	0.0005			< 0.0005

EXCEEDANCE SUMMARY

No exceedances are present above the regulatory limit(s) indicated



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Anions by discrete analyzer
Method: US EPA 375.4 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-026

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Sulphate	DIO5005-OCT24	mg/L	2	<2	0	20	106	80	120	104	75	125

Biochemical Oxygen Demand
Method: SM 5210 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-007

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Biochemical Oxygen Demand (BOD5)	BOD0015-OCT24	mg/L	2	< 2	2	30	97	70	130	86	70	130

Cyanide by SFA
Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-005

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Cyanide (total)	SKA0078-OCT24	mg/L	0.01	<0.01	ND	10	90	90	110	118	75	125



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Fluoride by Specific Ion Electrode
Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-014

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Fluoride	EWL0192-OCT24	mg/L	0.06	<0.06	ND	10	96	90	110	96	75	125

Mercury by CVAAS
Method: EPA 7471A/SM 3112B | Internal ref.: ME-CA-IENVISPE-LAK-AN-004

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Mercury (total)	EHG0019-OCT24	mg/L	0.00001	< 0.00001	ND	20	95	80	120	118	70	130



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Metals in aqueous samples - ICP-MS
Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-ENVISPE-LAK-AN-006

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Silver (total)	EMS0097-OCT24	mg/L	0.00005	<0.00005	ND	20	101	90	110	71	70	130
Aluminum (total)	EMS0097-OCT24	mg/L	0.001	<0.001	1	20	104	90	110	119	70	130
Arsenic (total)	EMS0097-OCT24	mg/L	0.0002	<0.0002	9	20	105	90	110	109	70	130
Cadmium (total)	EMS0097-OCT24	mg/L	0.000003	<0.000003	13	20	100	90	110	106	70	130
Cobalt (total)	EMS0097-OCT24	mg/L	0.000004	<0.000004	0	20	105	90	110	102	70	130
Chromium (total)	EMS0097-OCT24	mg/L	0.00008	<0.00008	5	20	105	90	110	98	70	130
Copper (total)	EMS0097-OCT24	mg/L	0.001	<0.001	ND	20	103	90	110	108	70	130
Manganese (total)	EMS0097-OCT24	mg/L	0.00001	<0.00001	1	20	104	90	110	104	70	130
Molybdenum (total)	EMS0097-OCT24	mg/L	0.0004	<0.0004	3	20	104	90	110	101	70	130
Nickel (total)	EMS0097-OCT24	mg/L	0.0001	<0.0001	ND	20	103	90	110	99	70	130
Lead (total)	EMS0097-OCT24	mg/L	0.00009	<0.00009	ND	20	102	90	110	101	70	130
Phosphorus (total)	EMS0097-OCT24	mg/L	0.003	<0.003	ND	20	98	90	110	NV	70	130
Antimony (total)	EMS0097-OCT24	mg/L	0.0009	<0.0009	ND	20	100	90	110	101	70	130
Selenium (total)	EMS0097-OCT24	mg/L	0.00004	<0.00004	16	20	102	90	110	106	70	130
Tin (total)	EMS0097-OCT24	mg/L	0.00006	<0.00006	6	20	109	90	110	NV	70	130
Titanium (total)	EMS0097-OCT24	mg/L	0.0001	<0.0001	ND	20	104	90	110	NV	70	130
Zinc (total)	EMS0097-OCT24	mg/L	0.002	<0.002	ND	20	104	90	110	104	70	130



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Nonylphenol and Ethoxylates

Method: ASTM D7065-06 | Internal ref.: ME-CA-IENVIGC-LAK-AN-015

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Nonylphenol diethoxylate	GCM0120-OCT24	mg/L	0.01	<0.01			81	55	120			
Nonylphenol monoethoxylate	GCM0120-OCT24	mg/L	0.01	<0.01			83	55	120			
Nonylphenol	GCM0120-OCT24	mg/L	0.001	<0.001			80	55	120			

Oil & Grease

Method: MOE E3401 | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Oil & Grease (total)	GCM0165-OCT24	mg/L	2	<2	NSS	20	106	75	125			



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Oil & Grease-AV/MS

Method: MOE E3401/SM 5520F | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Oil & Grease (animal/vegetable)	GCM0165-OCT24	mg/L	4	< 4	NSS	20	NA	70	130			
Oil & Grease (mineral/synthetic)	GCM0165-OCT24	mg/L	4	< 4	NSS	20	NA	70	130			

pH

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
pH	EWL0172-OCT24	No unit	0.05	NA	0		102			NA		

Phenols by SFA

Method: SM 5530B-D | Internal ref.: ME-CA-IENVISFA-LAK-AN-006

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
4AAP-Phenolics	SKA0089-OCT24	mg/L	0.002	<0.002	ND	10	98	80	120	96	75	125



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Polychlorinated Biphenyls

Method: MOE E3400/EPA 8082A | Internal ref.: ME-CA-IENVIGC-LAK-AN-001

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Polychlorinated Biphenyls (PCBs) - Total	GCM0142-OCT24	mg/L	0.0001	<0.0001	NSS	30	87	60	140	NSS	60	140

Semi-Volatile Organics

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Bis(2-ethylhexyl)phthalate	GCM0166-OCT24	mg/L	0.002	< 0.002	NSS	30	101	50	140	NSS	50	140
di-n-Butyl Phthalate	GCM0166-OCT24	mg/L	0.002	< 0.002	NSS	30	102	50	140	NSS	50	140



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-IENVIEWL-LAK-AN-004

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Total Suspended Solids	EWL0201-OCT24	mg/L	2	< 2	2	10	101	90	110	NA		

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Total Kjeldahl Nitrogen	SKA0080-OCT24	as N mg/L	0.5	<0.5	ND	10	103	90	110	105	75	125



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Volatile Organics
Method: EPA 5030B/8260C | Internal ref.: ME-CA-ENVIGC-LAK-AN-004

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
1,1,2,2-Tetrachloroethane	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	98	60	130	96	50	140
1,2-Dichlorobenzene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	100	60	130	88	50	140
1,4-Dichlorobenzene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	102	60	130	88	50	140
Benzene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	98	60	130	88	50	140
Chloroform	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	97	60	130	86	50	140
cis-1,2-Dichloroethylene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	99	60	130	89	50	140
Ethylbenzene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	100	60	130	92	50	140
m-p-xylene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	99	60	130	91	50	140
Methyl ethyl ketone	GCM0119-OCT24	mg/L	0.02	<0.02	ND	30	98	50	140	82	50	140
Methylene Chloride	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	99	60	130	87	50	140
o-xylene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	101	60	130	91	50	140
Styrene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	101	60	130	90	50	140
Tetrachloroethylene (perchloroethylene)	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	97	60	130	87	50	140
Toluene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	95	60	130	88	50	140
trans-1,3-Dichloropropene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	96	60	130	86	50	140
Trichloroethylene	GCM0119-OCT24	mg/L	0.0005	<0.0005	ND	30	100	60	130	84	50	140



FINAL REPORT

CA40064-OCT24 R1

QC SUMMARY

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Matrix Spike Qualifier: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

LEGEND

FOOTNOTES

NSS Insufficient sample for analysis.

RL Reporting Limit.

↑ Reporting limit raised.

↓ Reporting limit lowered.

NA The sample was not analysed for this analyte

ND Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

This document is issued, on the Client's behalf, by the Company under its General Conditions of Service available on request and accessible at http://www.sgs.com/terms_and_conditions.htm.

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This report supersedes all previous versions.

-- End of Analytical Report --



Request for Laboratory Services and CHAIN OF CUSTODY

Industries & Environment - Lakefield: 185 Concession St., Lakefield, ON K0L 2H0 Phone: 705-652-2000 Fax: 705-652-6365 Web: www.sgs.com/environment

- London: 657 Consortium Court, London, ON, N6E 2S8 Phone: 519-672-4500 Toll Free: 877-848-8060 Fax: 519-672-0361

No: 035639

Page of

Laboratory Information Section - Lab use only

Received By: Abneen
Received Date: 10/07/24 (mm/dd/yy)
Received Time: 16:00 (hr:min)

Received By (signature): [Signature]
Custody Seal Present: Yes ☒ No ☐
Custody Seal Intact: Yes ☒ No ☐

Cooling Agent Present: Yes ☒ No ☐ Type: ICE
Temperature Upon Receipt (°C): 9 x 3

LAB LIMS #: 40064

REPORT INFORMATION
Company: DS CONSULTANTS LTD.
Contact: DON HSU
Address: 6221 HWY 7-J16
VAUGHAN ON, L4H 0K8
Phone: 416 722 6247
Fax:
Email: dhsu@dsconsultants.co

INVOICE INFORMATION
☐ (same as Report Information)
Company:
Contact:
Address:
Phone:
Fax:

Quotation #:
Project #: 19-043-101
P.O. #:
Site Location/ID: 4721-5061 STOUFFVILLE
TURNAROUND TIME (TAT) REQUIRED RD.
☒ Regular TAT (5-7 days)
TAT's are quoted in business days (exclude statutory holidays & weekends).
Samples received after 6pm or on weekends: TAT begins next business day
RUSH TAT (Additional Charges May Apply): ☐ 1 Day ☐ 2 Days ☐ 3 Days ☐ 4 Days
PLEASE CONFIRM RUSH FEASIBILITY WITH SGS REPRESENTATIVE PRIOR TO SUBMISSION
Specify Due Date:
*NOTE: DRINKING (POTABLE) WATER SAMPLES FOR HUMAN CONSUMPTION MUST BE SUBMITTED WITH SGS DRINKING WATER CHAIN OF CUSTODY

REGULATIONS
☐ O.Reg 153/04 ☐ O.Reg 406/19
Other Regulations:
☐ Table 1 ☐ Res/Park ☐ Soil Texture:
☐ Table 2 ☐ Ind/Com ☐ Coarse
☐ Table 3 ☐ Agri/Other ☐ Medium/Fine
☐ Table ☐ Appx.
Soil Volume ☐ <350m3 ☐ >350m3
Sewer By-Law:
☒ Sanitary
☒ Storm
Municipality: YORK
☐ Reg 347/558 (3 Day min TAT)
☐ PWQO ☐ MMR
☐ CCME ☐ Other:
☐ MISA
☐ ODWS Not Reportable *See note

RECORD OF SITE CONDITION (RSC) ☐ YES ☒ NO

SAMPLE IDENTIFICATION	DATE SAMPLED	TIME SAMPLED	# OF BOTTLES	MATRIX
1 <u>BH 19-5</u>	<u>10/7/24</u>	<u>11:00</u>	<u>18</u>	<u>GW</u>
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				

ANALYSIS REQUESTED												
M & I		SVOC	PCB	PHC	VOC	Pest	Other (please specify)			SPLP	TCLP	COMMENTS:
Field Filtered (Y/N)	Metals & Inorganics <small>(incl CrVI, CN, Hg pH, B(HVWS), EC, SAR, soil) (CL, No-water)</small>									Specify tests	Specify tests	
	Full Metals Suite <small>(ICP metals plus B(HVWS-soil only) Hg, CrVI)</small>											
	ICP Metals only <small>Sb, As, Ba, Be, B, Cd, Cr, Co, Cu, Pb, Mo, Ni, Se, Ag, Ti, U, V, Zn</small>											
	PAHs only											
	SVOCs <small>all incl PAHs, ABNs, CPs</small>											
		PCBs	Total <input type="checkbox"/> Aroclor <input type="checkbox"/>	F1-F4 + BTEX	F1-F4 only <small>no BTEX</small>	VOCs <small>all incl BTEX</small>	BTEX only	Pesticides <small>Organochlorine or specify other</small>				

5 Day TAT

Observations/Comments/Special Instructions

Sampled By (NAME): DON HSU Signature: [Signature] Date: 10/7/24 (mm/dd/yy) Pink Copy - Client
Relinquished by (NAME): DON HSU Signature: [Signature] Date: 10/7/24 (mm/dd/yy) Yellow & White Copy - SGS



FINAL REPORT

CA40161-NOV24 R1

19-043-103, Hwy 48 & Stouffville Rd, Stouffville

Prepared for

DS Consultants



FINAL REPORT

CA40161-NOV24 R1

First Page

CLIENT DETAILS

Client DS Consultants

Address 6221 Highway 7 Unit 16
Vaughan, Ontario
L4H 0K8, Canada

Contact Dorothy Santos

Telephone 905-329-2735

Facsimile 905-264-2685

Email dsantos@dsconsultants.ca

Project 19-043-103, Hwy 48 & Stouffville Rd, Stouffville

Order Number

Samples Ground Water (1)

LABORATORY DETAILS

Project Specialist Jill Campbell, B.Sc.,GISAS

Laboratory SGS Canada Inc.

Address 185 Concession St., Lakefield ON, K0L 2H0

Telephone 2165

Facsimile 705-652-6365

Email jill.campbell@sgs.com

SGS Reference CA40161-NOV24

Received 11/15/2024

Approved 11/22/2024

Report Number CA40161-NOV24 R1

Date Reported 11/22/2024

COMMENTS

RL - SGS Reporting Limit

Nonylphenol Ethoxylates is the sum of nonylphenol monoethoxylate and nonylphenol diethoxylate.

Temperature of Sample upon Receipt: 9 degrees C

Cooling Agent Present: Yes

Custody Seal Present: Yes

Chain of Custody Number: 040723

SIGNATORIES

Jill Campbell, B.Sc.,GISAS



TABLE OF CONTENTS

First Page..... 1-2

Index..... 3

Results..... 4-7

Exceedance Summary..... 8

QC Summary..... 9-17

Legend..... 18

Annexes..... 19



FINAL REPORT

CA40161-NOV24 R1

Client: DS Consultants

Project: 19-043-103, Hwy 48 & Stouffville Rd, Stouffville

Project Manager: Dorothy Santos

Samplers: Chaitanya

MATRIX: WATER

Sample Number 8

Sample Name BH 24-5

Sample Matrix Ground Water

Sample Date 15/11/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102

L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
-----------	-------	----	----	----	--------

General Chemistry

Biochemical Oxygen Demand (BOD5)	mg/L	2	300	15	< 4 †
Total Suspended Solids	mg/L	2	350	15	3
Total Kjeldahl Nitrogen	as N mg/L	0.5	100	1	0.6

Metals and Inorganics

Sulphate	mg/L	2	1500		36
Cyanide (total)	mg/L	0.01	2	0.02	< 0.01
Fluoride	mg/L	0.06	10		0.11
Aluminum (total)	mg/L	0.001	50		0.056
Antimony (total)	mg/L	0.0009	5		< 0.0009
Arsenic (total)	mg/L	0.0002	1	0.02	0.0006
Cadmium (total)	mg/L	0.000003	0.7	0.008	0.000017
Chromium (total)	mg/L	0.00008	2	0.08	0.00045
Cobalt (total)	mg/L	0.000004	5		0.00126
Copper (total)	mg/L	0.001	3	0.05	0.001
Lead (total)	mg/L	0.00009	1	0.12	0.00069
Manganese (total)	mg/L	0.00001	5	0.15	0.323
Molybdenum (total)	mg/L	0.0004	5		0.0017
Nickel (total)	mg/L	0.0001	2	0.08	0.0047
Phosphorus (total)	mg/L	0.003	10	0.4	0.024
Selenium (total)	mg/L	0.00004	1	0.02	0.00017
Silver (total)	mg/L	0.00005	5	0.12	< 0.00005
Tin (total)	mg/L	0.00006	5		0.00173



FINAL REPORT

CA40161-NOV24 R1

Client: DS Consultants

Project: 19-043-103, Hwy 48 & Stouffville Rd, Stouffville

Project Manager: Dorothy Santos

Samplers: Chaitanya

MATRIX: WATER

Sample Number 8

Sample Name BH 24-5

Sample Matrix Ground Water

Sample Date 15/11/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102

L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
-----------	-------	----	----	----	--------

Metals and Inorganics (continued)

Titanium (total)	mg/L	0.0001	5		0.0023
Zinc (total)	mg/L	0.002	2	0.04	0.007

Nonylphenol and Ethoxylates

Nonylphenol	mg/L	0.001	0.02		< 0.001
Nonylphenol Ethoxylates	mg/L	0.01	0.2		< 0.01
Nonylphenol diethoxylate	mg/L	0.01			< 0.01
Nonylphenol monoethoxylate	mg/L	0.01			< 0.01

Oil and Grease

Oil & Grease (total)	mg/L	2			< 2
Oil & Grease (animal/vegetable)	mg/L	4	150		< 4
Oil & Grease (mineral/synthetic)	mg/L	4	15		< 4

Other (ORP)

pH	No unit	0.05	10.5	9	7.23
Mercury (total)	mg/L	0.00001	0.01	0.0004	< 0.00001



FINAL REPORT

CA40161-NOV24 R1

Client: DS Consultants

Project: 19-043-103, Hwy 48 & Stouffville Rd, Stouffville

Project Manager: Dorothy Santos

Samplers: Chaitanya

MATRIX: WATER

Sample Number 8

Sample Name BH 24-5

Sample Matrix Ground Water

Sample Date 15/11/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102

L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
PCBs					
Polychlorinated Biphenyls (PCBs) - Total	mg/L	0.0001	0.001	0.0004	< 0.0001
Phenols					
4AAP-Phenolics	mg/L	0.002	1	0.008	0.005
SVOCs					
di-n-Butyl Phthalate	mg/L	0.002	0.08	0.015	< 0.002
Bis(2-ethylhexyl)phthalate	mg/L	0.002	0.012	0.0088	< 0.002
VOCs					
Chloroform	mg/L	0.0005	0.04	0.002	< 0.0005
1,2-Dichlorobenzene	mg/L	0.0005	0.05	0.0056	< 0.0005
1,4-Dichlorobenzene	mg/L	0.0005	0.08	0.0068	< 0.0005
cis-1,2-Dichloroethylene	mg/L	0.0005	4	0.0056	< 0.0005
trans-1,3-Dichloropropene	mg/L	0.0005	0.14	0.0056	< 0.0005
Methylene Chloride	mg/L	0.0005	2	0.0052	< 0.0005
1,1,2,2-Tetrachloroethane	mg/L	0.0005	1.4	0.017	< 0.0005
Tetrachloroethylene (perchloroethylene)	mg/L	0.0005	1	0.0044	< 0.0005
Trichloroethylene	mg/L	0.0005	0.4	0.008	< 0.0005
Methyl ethyl ketone	mg/L	0.02	8		< 0.02
Styrene	mg/L	0.0005	0.2		< 0.0005



FINAL REPORT

CA40161-NOV24 R1

Client: DS Consultants
Project: 19-043-103, Hwy 48 & Stouffville Rd, Stouffville
Project Manager: Dorothy Santos
Samplers: Chaitanya

MATRIX: WATER

Sample Number 8
Sample Name BH 24-5
Sample Matrix Ground Water
Sample Date 15/11/2024

L1 = SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102
L2 = SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102

Parameter	Units	RL	L1	L2	Result
VOCs - BTEX					
Benzene	mg/L	0.0005	0.01	0.002	< 0.0005
Ethylbenzene	mg/L	0.0005	0.16	0.002	< 0.0005
Toluene	mg/L	0.0005	0.27	0.002	< 0.0005
Xylene (total)	mg/L	0.0005	1.4	0.0044	< 0.0005
m-p-xylene	mg/L	0.0005			< 0.0005
o-xylene	mg/L	0.0005			< 0.0005



EXCEEDANCE SUMMARY

				SANSEW / WATER / - - York Sewer Use ByLaw - Sanitary Sewer Discharge - BL_2021_102	SANSEW / WATER / - - York Sewer Use ByLaw - Storm Sewer Discharge - BL_2021_102
Parameter	Method	Units	Result	L1	L2

BH 24-5

Manganese	SM 3030/EPA 200.8	mg/L	0.323
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0.15



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Anions by discrete analyzer
Method: US EPA 375.4 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-026

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Sulphate	DIO8029-NOV24	mg/L	2	<2	1	20	102	80	120	104	75	125

Biochemical Oxygen Demand
Method: SM 5210 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-007

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Biochemical Oxygen Demand (BOD5)	BOD0029-NOV24	mg/L	2	< 2	6	30	86	70	130	82	70	130

Cyanide by SFA
Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-005

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Cyanide (total)	SKA0162-NOV24	mg/L	0.01	<0.01	1	10	105	90	110	88	75	125



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Fluoride by Specific Ion Electrode
Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-014

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Fluoride	EWL0467-NOV24	mg/L	0.06	<0.06	ND	10	101	90	110	90	75	125

Mercury by CVAAS
Method: EPA 7471A/SM 3112B | Internal ref.: ME-CA-IENVISPE-LAK-AN-004

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Mercury (total)	EHG0046-NOV24	mg/L	0.00001	< 0.00001	ND	20	116	80	120	111	70	130



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Metals in aqueous samples - ICP-MS
Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-ENVISPE-LAK-AN-006

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Tin (total)	EMS0202-NOV24	mg/L	0.00006	<0.00006	1	20	99	90	110	NV	70	130
Titanium (total)	EMS0202-NOV24	mg/L	0.0001	<0.0001	ND	20	98	90	110	NV	70	130
Zinc (total)	EMS0202-NOV24	mg/L	0.002	<0.002	2	20	98	90	110	118	70	130
Silver (total)	EMS0202-NOV24	mg/L	0.00005	<0.00005	ND	20	95	90	110	88	70	130
Aluminum (total)	EMS0202-NOV24	mg/L	0.001	<0.001	1	20	103	90	110	109	70	130
Arsenic (total)	EMS0202-NOV24	mg/L	0.0002	<0.0002	ND	20	101	90	110	109	70	130
Cadmium (total)	EMS0202-NOV24	mg/L	0.000003	<0.000003	0	20	100	90	110	105	70	130
Cobalt (total)	EMS0202-NOV24	mg/L	0.000004	<0.000004	7	20	100	90	110	109	70	130
Chromium (total)	EMS0202-NOV24	mg/L	0.00008	<0.00008	2	20	102	90	110	107	70	130
Copper (total)	EMS0202-NOV24	mg/L	0.001	<0.001	1	20	101	90	110	115	70	130
Manganese (total)	EMS0202-NOV24	mg/L	0.00001	<0.00001	7	20	103	90	110	126	70	130
Molybdenum (total)	EMS0202-NOV24	mg/L	0.0004	<0.0004	6	20	101	90	110	109	70	130
Nickel (total)	EMS0202-NOV24	mg/L	0.0001	<0.0001	3	20	98	90	110	102	70	130
Lead (total)	EMS0202-NOV24	mg/L	0.00009	<0.00009	4	20	96	90	110	103	70	130
Phosphorus (total)	EMS0202-NOV24	mg/L	0.003	<0.003	0	20	102	90	110	NV	70	130
Antimony (total)	EMS0202-NOV24	mg/L	0.0009	<0.0009	ND	20	103	90	110	102	70	130
Selenium (total)	EMS0202-NOV24	mg/L	0.00004	<0.00004	ND	20	102	90	110	117	70	130



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Nonylphenol and Ethoxylates

Method: ASTM D7065-06 | Internal ref.: ME-CA-IENVIGC-LAK-AN-015

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Nonylphenol diethoxylate	GCM0320-NOV24	mg/L	0.01	<0.01			88	55	120			
Nonylphenol monoethoxylate	GCM0320-NOV24	mg/L	0.01	<0.01			87	55	120			
Nonylphenol	GCM0320-NOV24	mg/L	0.001	<0.001			84	55	120			

Oil & Grease

Method: MOE E3401 | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Oil & Grease (total)	GCM0325-NOV24	mg/L	2	<2	NSS	20	97	75	125			



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Oil & Grease-AV/MS

Method: MOE E3401/SM 5520F | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Oil & Grease (animal/vegetable)	GCM0325-NOV24	mg/L	4	< 4	NSS	20	NA	70	130			
Oil & Grease (mineral/synthetic)	GCM0325-NOV24	mg/L	4	< 4	NSS	20	NA	70	130			

pH

Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
pH	EWL0360-NOV24	No unit	0.05	NA	0		100			NA		

Phenols by SFA

Method: SM 5530B-D | Internal ref.: ME-CA-IENVISFA-LAK-AN-006

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
4AAP-Phenolics	SKA0191-NOV24	mg/L	0.002	<0.002	ND	10	96	80	120	NV	75	125



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Polychlorinated Biphenyls

Method: MOE E3400/EPA 8082A | Internal ref.: ME-CA-IENVIGC-LAK-AN-001

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Polychlorinated Biphenyls (PCBs) - Total	GCM0323-NOV24	mg/L	0.0001	<0.0001	NSS	30	75	60	140	NSS	60	140

Semi-Volatile Organics

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Bis(2-ethylhexyl)phthalate	GCM0285-NOV24	mg/L	0.002	< 0.002	NSS	30	105	50	140	NSS	50	140
di-n-Butyl Phthalate	GCM0285-NOV24	mg/L	0.002	< 0.002	NSS	30	107	50	140	NSS	50	140



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-IENVIEWL-LAK-AN-004

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Total Suspended Solids	EWL0355-NOV24	mg/L	2	< 2	3	10	93	90	110	NA		

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
Total Kjeldahl Nitrogen	SKA0184-NOV24	as N mg/L	0.5	<0.5	2	10	103	90	110	98	75	125



FINAL REPORT

CA40161-NOV24 R1

QC SUMMARY

Volatile Organics

Method: EPA 5030B/8260C | Internal ref.: ME-CA-IENVIGC-LAK-AN-004

Parameter	QC batch Reference	Units	RL	Method Blank	Duplicate		LCS/Spike Blank			Matrix Spike / Ref.		
					RPD	AC (%)	Spike Recovery (%)	Recovery Limits (%)		Spike Recovery (%)	Recovery Limits (%)	
								Low	High		Low	High
1,1,2,2-Tetrachloroethane	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	95	60	130	87	50	140
1,2-Dichlorobenzene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	99	60	130	94	50	140
1,4-Dichlorobenzene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	97	60	130	93	50	140
Benzene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	99	60	130	97	50	140
Chloroform	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	99	60	130	94	50	140
cis-1,2-Dichloroethylene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	98	60	130	96	50	140
Ethylbenzene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	103	60	130	100	50	140
m-p-xylene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	104	60	130	100	50	140
Methyl ethyl ketone	GCM0301-NOV24	mg/L	0.02	<0.02	ND	30	87	50	140	91	50	140
Methylene Chloride	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	95	60	130	89	50	140
o-xylene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	103	60	130	99	50	140
Styrene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	104	60	130	100	50	140
Tetrachloroethylene (perchloroethylene)	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	97	60	130	94	50	140
Toluene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	98	60	130	94	50	140
trans-1,3-Dichloropropene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	100	60	130	94	50	140
Trichloroethylene	GCM0301-NOV24	mg/L	0.0005	<0.0005	ND	30	99	60	130	93	50	140

QC SUMMARY

Method Blank: a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

Duplicate: Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

LCS/Spike Blank: Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

Reference Material: a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

RL: Reporting limit

RPD: Relative percent difference

AC: Acceptance criteria

Multielement Scan Qualifier: as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

Duplicate Qualifier: for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Matrix Spike Qualifier: for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

LEGEND

FOOTNOTES

NSS Insufficient sample for analysis.

RL Reporting Limit.

↑ Reporting limit raised.

↓ Reporting limit lowered.

NA The sample was not analysed for this analyte

ND Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

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This report supersedes all previous versions.

-- End of Analytical Report --



Appendix D



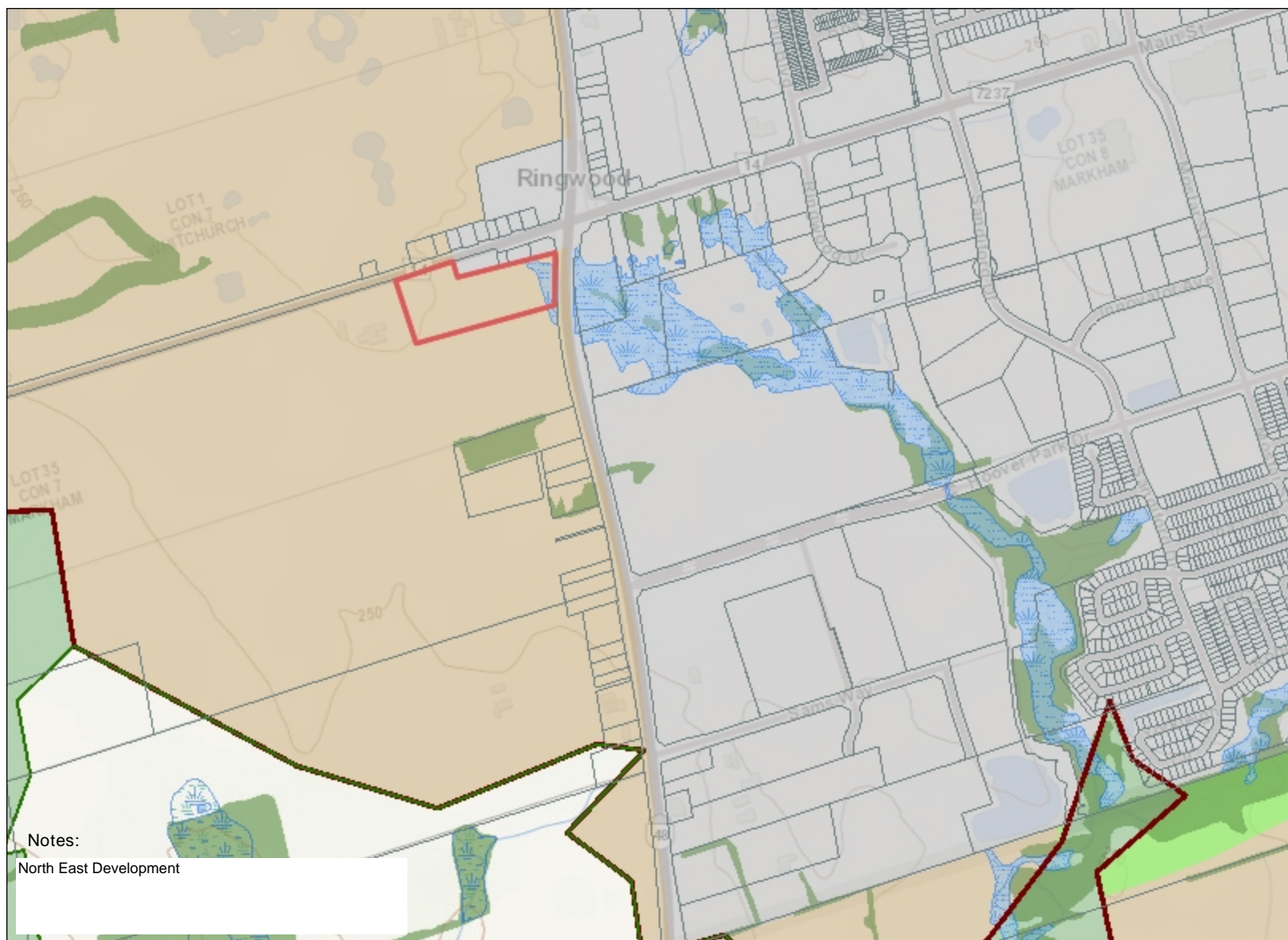
MECP Water Well Record Search - 500 m of site

TOWNSHIP	UTM	E	N	DATE CNTR	CASING	WATER	PUMP TEST	WELL USE	SCREEN	WELL	WELL TAG	FORMATION
WHITCHURCH-STOUFFVIL CON 08 001	17 W	638015	4869363	1976/11 3109	30 24	FR 0066	25///:	DO		6913849		LOAM 0002 BRWN CLAY 0022 BLUE CLAY STNY 0047 SAND 0050 BLUE CLAY STNY 0065 GRVL 0070
WHITCHURCH-STOUFFVIL CON 08 001	17 W	637925	4869623	1970/05 5459	5	FR 0046	0/48/3/6:0	DO	0048 4	6909955		PRDG 0017 GREY CLAY GRVL 0035 GREY GRVL CLAY BLDR 0046 GREY MSND 0052
WHITCHURCH-STOUFFVIL CON 08 001	17 W	638124	4869457	1950/11 2204	2	FR 0047		ST DO		6908178		BLUE CLAY 0047
STOUFFVILLE VILLAGE	17 W	637849	4869254	2007/09 7241	1.5			TH		7051198	(Z63654) A063681	BRWN FILL SAND LOOS 0003 BRWN CLAY SILT SOFT 0008 GREN CLAY SILT DNSE 0011 GREY CLAY SILT 0016
WHITCHURCH-STOUFFVIL CON 08 001	17 W	637999	4869455	1952/07 2204	2	FR 0052	1/15/6/:	DO		6908176		PRDG 0020 BLUE CLAY STNS 0052 GRVL 0053
STOUFFVILLE VILLAGE	17 W	637852	4869248	2009/06 7241	5.19			MT	0010 10	7126408	(Z100258) A086578	BRWN FILL SAND GRVL 0004 BRWN SAND SILT DNSE 0012 GREY CLAY SILT WBRG 0020
STOUFFVILLE VILLAGE	17 W	637868	4869236	2009/06 7241	5.19			MT	0010 10	7126409	(Z100255) A086579	BRWN FILL SAND GRVL 0004 BRWN SAND SILT DNSE 0012 GREY CLAY SILT WBRG 0020
STOUFFVILLE VILLAGE	17 W	637834	4869224	2009/06 7241	2.04			MT	0010 10	7126411	(Z100256) A086581	BRWN FILL SAND GRVL 0004 BRWN SAND SILT DNSE 0012 GREY CLAY SILT WBRG 0020
STOUFFVILLE VILLAGE	17 W	637834	4869224	2009/10 7241	2.04			MT	0010 10	7133785	(Z104753) A086581 A	
STOUFFVILLE VILLAGE	17 W	637868	4869247	2009/10 7241	2.04			MT	0010 10	7133786	(Z104750) A086580 A	
STOUFFVILLE VILLAGE	17 W	637852	4869248	2009/10 7241	2.04			MT	0010 10	7133787	(Z104749) A086578 A	
STOUFFVILLE VILLAGE	17 W	637868	4869236	2009/10 7241	2.04			MT	0010 10	7133788	(Z104751) A086579 A	
STOUFFVILLE VILLAGE	17 W	637868	4869247	2009/06 7241	2.04			MT	0007 10	7126410	(Z100257) A086580	BRWN FILL SAND GRVL 0008 BRWN SAND SILT DNSE 0012 GREY CLAY SILT DNSE 0017
WHITCHURCH-STOUFFVIL CON 08 035	17 W	638062	4869328	1949/08 2204	2	FR 0050	0//4/:	DO	0051 5	6904046		MSND CLAY 0030 BLUE CLAY 0050 BRWN CSND 0056
WHITCHURCH-STOUFFVIL CON 08 035	17 W	638015	4869012	1954/10 1622	4	FR 0050	5/20/10/10:0	DO	0053 4	6904048		FILL 0005 YLLW CLAY MSND STNS 0020 BLUE CLAY STNS 0050 YLLW MSND STNS 0057
WHITCHURCH-STOUFFVIL	17 W	637886	4868759	2006/06 7082	1.97			NU	0013 5	6930598	(Z23579) A023342	GRVL SAND 0003 BRWN CLAY SILT 0008 BRWN SAND SILT GRVL 0020
WHITCHURCH-STOUFFVIL CON 08 035	17 W	638318	4869415	1954/12 2419	2	FR 0055	//3/:	DO	0050 5	6904049		CLAY 0045 MSND 0055
WHITCHURCH-STOUFFVIL	17 W	637886	4868759	2006/11 7082						7046164	(Z70724) A023342 A	
WHITCHURCH-STOUFFVIL CON 08 035	17 W	638203	4869401	1960/06 5420	34	FR 0038	18//4/:	DO		6904051		YLLW CLAY 0003 BLUE CLAY 0038 BLUE CLAY GRVL 0040
WHITCHURCH-STOUFFVIL	17 W	637862	4869240	2007/06 6490	1.97				0010 10	7047744	(Z52236) A046388	BRWN SAND GRVL FILL 0009 GREY SILT CLAY SAND 0016 BRWN SAND WBRG 0020
WHITCHURCH-STOUFFVIL CON 08 035	17 W	637974	4869174	1960/12 2204	2	FR 0048	4/10/2/18:0	DO	0047 9	6904052		CLAY STNS 0032 GRVL 0033 CLAY STNS 0046 CSND 0056
WHITCHURCH-STOUFFVIL	17 W	638090	4869523	2014/12 7247	2	UT 0008		MT	0010 10	7239494	(Z198477) A174028	BRWN GRVL SAND FILL 0008 BRWN SILT SNDRY 0012 GREY TILL CLAY SAND 0020
WHITCHURCH-STOUFFVIL CON 08 035	17 W	638245	4869409	1961/01 2204	2	FR 0058	7///:	DO		6904053		PRDG 0020 BLUE CLAY STNS 0058 CSND 0059
WHITCHURCH-STOUFFVIL CON 08 035	17 W	638075	4869303	1976/12 1350	6	FR 0045	5/45/4/1:0	DO	0045 5	6913779		GREY CLAY 0021 GREY SILT 0027 GREY CLAY GRVL 0045 GREY GRVL CLAY 0050
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637590	4869587	2016/02 1413	5		7///:			7261539	(Z227322) A	
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637873	4869454	1993/03 1413	6 6	FR 0268	96/240/40/1:0	CO PS	0265 3	6922203		BRWN CLAY DNSE 0012 GREY CLAY STNS BLDR 0203 GREY CLAY DNSE 0212 GREY CLAY SILT SOFT 0230 GREY CLAY SAND DNSE 0263 BLCK GRVL SAND CLN 0269
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637775	4869283	1972/07 1350	6	FR 0036	3/14/10/2:20	DO		6911103		BRWN CLAY GRVL FILL 0003 BRWN CLAY 0015 BRWN GRVL CLAY 0017 GREY CLAY GRVL 0031 GREY GRVL CLAY 0036 BRWN GRVL CSND 0038
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637655	4869233	1971/12 2218	2	FR 0042	2///:	DO		6910791		BRWN CLAY STNS 0042 BRWN MSND CLAY 0070

WHITCHURCH-STOUFFVIL CON 07 001	17 W	637715	4869263	1976/03 5459	6	FR 0050	3/50/3/4:0	DO	0051 3	6913629		BRWN CLAY SAND 0018 BLUE CLAY STNS 0050 BLUE SAND GRVL STNS 0054
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637819	4869326	1964/05 2204	2	FR 0036	4/4/4/5:30	DO	0035 5	6908031		RED CLAY STNS 0030 BLUE CLAY 0036 CSND 0040
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637635	4869223	1978/08 5459	6	FR 0058	6/50/2/:	DO		6915056		LOAM 0003 BLUE CLAY 0018 BLUE CLAY HARD 0077
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637728	4869249	2005/07 1350				DO		6929288	(Z31519) A029430 A	BRWN CLAY 0006 YLLW CLAY GRVL STNS 0012 GREY CLAY GRVL BLDR 0085
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637762	4869295	1950/05 2419	2	FR 0060	3///:	DO		6908028		CLAY 0020 BLUE CLAY 0040 CLAY GRVL 0050 MSND GRVL 0060
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637595	4869213	1969/10 5420	34	FR 0017	3///:	DO		6909699		LOAM 0001 BRWN CLAY MSND 0012 BLUE CLAY 0017 BRWN MSND 0020
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637681	4869301	1957/05 2204	2	FR 0052	3/10/3/0:30	PS		6908029		MSND CLAY 0030 BLUE CLAY STNS 0052
WHITCHURCH-STOUFFVIL CON 07 001	17 W	637587	4869271	1958/09 2204	2	FR 0052	8/12/2/96:0	DO	0047 5	6908030		CLAY 0040 BLUE CLAY STNS 0049 GRVL CLAY 0052
WHITCHURCH-STOUFFVIL CON 07 034	17 W	637936	4868827	1962/11 5420	34	FR 0020	20///:	DO		6903949		LOAM 0001 YLLW CLAY 0008 CLAY MSND 0018 CSND 0020 BLUE CLAY 0030
WHITCHURCH-STOUFFVIL CON 07 035	17 W	637863	4869280	1986/05 5459	6	FR 0192	106/185/10/2:0	DO	0192 6	6918625		BRWN SAND FILL 0005 BLUE CLAY STNS 0049 BLUE SAND CLAY 0062 BLUE CLAY HARD 0091 BLUE CLAY STNS 0115 BLUE CLAY HARD 0170 BLUE CLAY SOFT 0192 BLCK CSND 0195 BLUE SAND CLAY 0198
WHITCHURCH-STOUFFVIL CON 07 035	17 W	637755	4869223	1981/08 2218	2	FR 0042	-4//2/48:30		0051 14	6915909		BRWN CLAY STNS 0042 BLUE CLAY SAND 0065
WHITCHURCH-STOUFFVIL CON 07 035	17 W	637527	4869062	2014/10 3108						7234034	(Z162204) A	
WHITCHURCH-STOUFFVIL CON 07 035	17 W	637619	4869132	1961/04 5420	34	FR 0013	13//2/:	ST DO		6903954		LOAM 0001 YLLW CLAY MSND 0010 CSND 0020
WHITCHURCH-STOUFFVIL CON 07 035	17 W	637535	4869016	1999/01 6874	3	FR 0019	13/14/25/2:0	DO		6924779		SAND 0010 BRWN SAND 0019
WHITCHURCH-STOUFFVIL CON 07 035	17 W	637730	4869234	1961/07 2204	2	FR 0020	4/34/2/12:0	DO	0035 5	6903955		PRDG 0020 CLAY STNS 0034 GRVL 0040
WHITCHURCH-STOUFFVIL CON 08 001	17 W	637996	4869374	1957/11 2204	2	FR 0041	4///:	DO		6908179		PRDG 0022 CLAY STNS 0043 GRVL 0044
WHITCHURCH-STOUFFVIL CON 08 001	17 W	637959	4869329	2009/01 5459						7130184	(Z101450) A075302 A	



Appendix E



Notes:
North East Development

0.7 0 0.33 0.7 Kilometres

This map should not be relied on as a precise indicator of routes or locations, nor as a guide to navigation. The Ontario Ministry of Natural Resources and Forestry(OMNRF) shall not be liable in any way for the use of, or reliance upon, this map or any information on this map.

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Legend

-  Assessment Parcel
-  Greenbelt Area Boundary
-  ORM Boundary
-  NEP Boundary
-  NEP Parks and Open Space System
- ANSI
-  Earth Science Provincially Significant/sciences de la terre d'importance provinciale
-  Earth Science Regionally Significant/sciences de la terre d'importance régionale
-  Life Science Provincially Significant/sciences de la vie d'importance provinciale
-  Life Science Regionally Significant/sciences de la vie d'importance régionale
-  Evaluated Wetland
-  Provincially Significant/considérée d'importance provinciale
-  Non-Provincially Significant/non considérée d'importance provinciale
-  Unevaluated Wetland
-  Woodland
-  Conservation Reserve
-  Provincial Park
-  Greenbelt Towns and Villages
- ORM Land Use Designation
-  Countryside Area/zona de campagne
-  Natural Core Area/zona centrale naturelle
-  Natural Linkage Area/liens naturel
-  Palgrave Estates Residential Community/communauté résidentielle de Palgrave Estates
-  Rural Settlement/zona de peuplement rurale
-  Settlement Area/zona de peuplement
- NEP Land Use Designation
-  Escarpment Natural Area/zona naturelle de l'escarpement
-  Escarpment Protection Area/zona protégée de l'escarpement
-  Escarpment Recreation Area/zona récréative de l'escarpement
-  Escarpment Rural Area/zona rurale de l'escarpement
-  Mineral Resource Extraction Area/zona d'extraction de ressources minérales
-  Urban Area/zona urbaine
-  Natural Heritage System





Appendix F

TABLE 1
CLIMATE NORMALS 1981-2010 (Richmond Hill Climate Station)
Water Balance - 5061 Stouffvill Road, Whitchurch-Stouffville, ON

Month	Thornthwaite (1948)					
	Mean Temperature (°C)	Heat Index	Unadjusted Potential Evapotranspiration (mm)	Daylight Correction Value	Adjusted Potential Evapotranspiration (mm)	Total Precipitation (mm)
January	-6.2	0.0	0.0	0.81	0.0	62.3
February	-4.9	0.0	0.0	0.82	0.0	58.0
March	-0.3	0.0	0.0	1.02	0.0	58.8
April	6.9	1.6	29.9	1.12	33.4	70.1
May	13.3	4.4	62.2	1.26	78.3	81.6
June	18.7	7.4	91.0	1.28	116.5	80.2
July	21.4	9.0	105.8	1.29	136.5	83.5
August	20.3	8.3	99.8	1.20	119.7	89.2
September	15.9	5.8	75.9	1.04	79.0	88.4
October	9.1	2.5	40.7	0.95	38.6	69.1
November	3.1	0.5	12.2	0.81	9.9	87.2
December	-2.7	0.0	0.0	0.77	0.0	66.8
TOTALS		39.5	517.4		612.0	895.2

Notes: Daylight Correction values obtained from Instruction and Tables For Computing Potential Evapotranspiration and The Water Balance (Thornthwaite & Mather, 1957)

TABLE 2

Pre-development Water Balance

Water Balance - 5061 Stouffville Road, Whitchurch-Stouffville, ON

Catchments and Hydrologic Components			Month												Total
			March	April	May	June	July	August	September	October	November	December	January	February	
PET - Adjusted Potential Evapotranspiration (mm)			0.00	33.44	78.34	116.49	136.51	119.71	78.95	38.64	9.88	0.00	0.00	0.00	611.96
P - Total Precipitation (mm)			58.80	70.10	81.60	80.20	83.50	89.20	88.40	69.10	87.20	66.80	62.30	58.00	895.20
P-PET (mm)			58.80	36.66	3.26	-36.29	-53.01	-30.51	9.45	30.46	77.32	66.80	62.30	58.00	-
Soil Moisture Deficit (mm)			0.00	0.00	0.00	-36.29	-89.30	-119.80	-110.36	-79.90	-2.58	0.00	0.00	0.00	-
Site	Agricultural/Moderately Rooted Crop (Catchment 304)	Soil Moisture Storage (mm)	200.00	200.00	200.00	163.71	110.70	80.20	89.64	120.10	197.42	200.00	200.00	200.00	-
		Actual Potential Evapotranspiration (mm)	0.00	33.44	78.34	113.20	119.86	103.76	78.95	38.64	9.88	0.00	0.00	0.00	576.08
		P-AET (mm)	58.80	36.66	3.26	-33.00	-36.36	-14.56	9.45	30.46	77.32	66.80	62.30	58.00	-
		Actual Soil Moisture Deficit (mm)	0.00	0.00	0.00	-33.00	-69.36	-83.92	-74.47	-44.02	0.00	0.00	0.00	0.00	-
		Change in Soil Moisture Deficit (mm)	0.00	0.00	0.00	33.00	36.36	14.56	-9.45	-30.46	-44.02	0.00	0.00	0.00	-
		Precipitation Surplus (mm)	58.80	36.66	3.26	0.00	0.00	0.00	0.00	0.00	33.30	66.80	62.30	58.00	319.12
		MECP Infiltration Factor	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	-
		Run-Off Coefficient	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	-
		Infiltration (mm)	35.28	22.00	1.95	0.00	0.00	0.00	0.00	0.00	19.98	40.08	37.38	34.80	191.47
		Run-Off (mm)	23.52	14.67	1.30	0.00	0.00	0.00	0.00	0.00	13.32	26.72	24.92	23.20	127.65
	Catchment Area (m ²) = 14342.00		Monthly Volumes												
	Total AET (m ³)		0.00	479.53	1123.58	1623.48	1719.09	1488.12	1132.31	554.24	141.77	0.00	0.00	0.00	8262.13
	Total Evaporation (m ³)		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	Total Infiltration (m ³)		505.99	315.51	28.03	0.00	0.00	0.00	0.00	0.00	286.54	574.83	536.10	499.10	2746.10
	Total Runoff (m ³)		337.32	210.34	18.69	0.00	0.00	0.00	0.00	0.00	191.02	383.22	357.40	332.73	1830.73
	Agricultural/Moderately Rooted Crop (Catchment 305)	Soil Moisture Storage (mm)	200.00	200.00	200.00	163.71	110.70	80.20	89.64	120.10	197.42	200.00	200.00	200.00	-
		Actual Potential Evapotranspiration (mm)	0.00	33.44	78.34	113.20	119.86	103.76	78.95	38.64	9.88	0.00	0.00	0.00	576.08
		P-AET (mm)	58.80	36.66	3.26	-33.00	-36.36	-14.56	9.45	30.46	77.32	66.80	62.30	58.00	-
		Actual Soil Moisture Deficit (mm)	0.00	0.00	0.00	-33.00	-69.36	-83.92	-74.47	-44.02	0.00	0.00	0.00	0.00	-
		Change in Soil Moisture Deficit (mm)	0.00	0.00	0.00	33.00	36.36	14.56	-9.45	-30.46	-44.02	0.00	0.00	0.00	-
		Precipitation Surplus (mm)	58.80	36.66	3.26	0.00	0.00	0.00	0.00	0.00	33.30	66.80	62.30	58.00	319.12
		MECP Infiltration Factor	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	-
		Run-Off Coefficient	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	-
		Infiltration (mm)	35.28	22.00	1.95	0.00	0.00	0.00	0.00	0.00	19.98	40.08	37.38	34.80	191.47
		Run-Off (mm)	23.52	14.67	1.30	0.00	0.00	0.00	0.00	0.00	13.32	26.72	24.92	23.20	127.65
	Catchment Area (m ²) = 12406.00		Monthly Volumes												
	Total AET (m ³)		0.00	414.80	971.91	1404.33	1487.04	1287.24	979.46	479.42	122.63	0.00	0.00	0.00	7146.84
	Total Evaporation (m ³)		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	Total Infiltration (m ³)		437.68	272.92	24.25	0.00	0.00	0.00	0.00	0.00	247.86	497.23	463.74	431.73	2375.41
	Total Runoff (m ³)		291.79	181.94	16.17	0.00	0.00	0.00	0.00	0.00	165.24	331.49	309.16	287.82	1583.60
	Site Total Monthly Volumes														
	Total AET (m ³)		0.00	894.33	2095.49	3027.81	3206.13	2775.37	2111.77	1033.66	264.40	0.00	0.00	0.00	15409
	Total Evaporation (m ³)		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0
	Total Infiltration (m ³)		943.67	588.42	52.29	0.00	0.00	0.00	0.00	0.00	534.39	1072.06	999.84	930.83	5122
	Total Runoff (m ³)		629.11	392.28	34.86	0.00	0.00	0.00	0.00	0.00	356.26	714.71	666.56	620.55	3414



TABLE 3

Post-development Water Balance

Water Balance - 5061 Stouffville Road, Whitchurch-Stouffville, ON

Catchments and Hydrologic Components			Month											Total		
			March	April	May	June	July	August	September	October	November	December	January		February	
PET - Adjusted Potential Evapotranspiration (mm)			0.00	33.44	78.34	116.49	136.51	119.71	78.95	38.64	9.88	0.00	0.00	0.00	611.96	
P - Total Precipitation (mm)			58.80	70.10	81.60	80.20	83.50	89.20	88.40	69.10	87.20	66.80	62.30	58.00	895.20	
P-PET (mm)			58.80	36.66	3.26	-36.29	-53.01	-30.51	9.45	30.46	77.32	66.80	62.30	58.00	-	
Soil Moisture Deficit (mm)			0.00	0.00	0.00	-36.29	-89.30	-119.80	-110.36	-79.90	-2.58	0.00	0.00	0.00	-	
Site	Catchment 304- Landscaped	Soil Moisture Storage (mm)	125.00	125.00	125.00	88.71	35.70	5.20	14.64	45.10	122.42	125.00	125.00	125.00	-	
		Actual Potential Evapotranspiration (mm)	0.00	33.44	78.34	111.22	109.88	94.19	78.95	38.64	9.88	0.00	0.00	0.00	554.55	
		P-AET (mm)	58.80	36.66	3.26	-31.02	-26.38	-4.99	9.45	30.46	77.32	66.80	62.30	58.00	-	
		Actual Soil Moisture Deficit (mm)	0.00	0.00	0.00	-31.02	-57.40	-62.39	-52.94	-22.49	0.00	0.00	0.00	0.00	-	
		Change in Soil Moisture Deficit (mm)	0.00	0.00	0.00	31.02	26.38	4.99	-9.45	-30.46	-22.49	0.00	0.00	0.00	-	
		Precipitation Surplus (mm)	58.80	36.66	3.26	0.00	0.00	0.00	0.00	0.00	54.83	66.80	62.30	58.00	340.65	
		MECP Infiltration Factor	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	-	
		Run-Off Coefficient	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	-	
		Infiltration (mm)	35.28	22.00	1.95	0.00	0.00	0.00	0.00	0.00	32.90	40.08	37.38	34.80	204.39	
		Run-Off (mm)	23.52	14.67	1.30	0.00	0.00	0.00	0.00	0.00	21.93	26.72	24.92	23.20	136.26	
		Catchment Area* (m ²) = 4131.00	Monthly Volumes													
	Catchment 304(Developme nt)	Precipitation (mm)	58.80	70.10	81.60	80.20	83.50	89.20	88.40	69.10	87.20	66.80	62.30	58.00	895.20	
		Evaporation Factor	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	-	
		Run-Off Coefficient	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	-	
		Evaporation (mm)	8.82	10.52	12.24	12.03	12.53	13.38	13.26	10.37	13.08	10.02	9.35	8.70	134.28	
		Run-Off (mm)	49.98	59.59	69.36	68.17	70.98	75.82	75.14	58.74	74.12	56.78	52.96	49.30	760.92	
		Catchment Area (m ²) = 10211.00	Monthly Volumes													
	Catchment 305- Landscaped	Total AET (m ³)	0.00	138.12	323.63	459.46	453.91	389.10	326.14	159.64	40.83	0.00	0.00	0.00	2290.84	
		Total Evaporation (m ³)	90.06	107.37	124.98	122.84	127.89	136.62	135.40	105.84	133.56	102.31	95.42	88.84	1371.13	
		Total Infiltration (m ³)	145.74	90.88	8.08	0.00	0.00	0.00	0.00	0.00	135.90	165.57	154.42	143.76	844.34	
		Total Runoff (m ³)	607.51	669.01	713.62	696.08	724.73	774.20	767.25	599.74	847.44	690.16	643.67	599.24	8332.64	
		Soil Moisture Storage (mm)	125.00	125.00	125.00	88.71	35.70	5.20	14.64	45.10	122.42	125.00	125.00	125.00	-	
		Actual Potential Evapotranspiration (mm)	0.00	33.44	78.34	111.22	109.88	94.19	78.95	38.64	9.88	0.00	0.00	0.00	554.55	
		P-AET (mm)	58.80	36.66	3.26	-31.02	-26.38	-4.99	9.45	30.46	77.32	66.80	62.30	58.00	-	
		Actual Soil Moisture Deficit (mm)	0.00	0.00	0.00	-31.02	-57.40	-62.39	-52.94	-22.49	0.00	0.00	0.00	0.00	-	
		Change in Soil Moisture Deficit (mm)	0.00	0.00	0.00	31.02	26.38	4.99	-9.45	-30.46	-22.49	0.00	0.00	0.00	-	
		Precipitation Surplus (mm)	58.80	36.66	3.26	0.00	0.00	0.00	0.00	0.00	54.83	66.80	62.30	58.00	340.65	
		MECP Infiltration Factor	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	0.60	-	
		Run-Off Coefficient	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	-	
		Infiltration (mm)	35.28	22.00	1.95	0.00	0.00	0.00	0.00	0.00	32.90	40.08	37.38	34.80	204.39	
		Run-Off (mm)	23.52	14.67	1.30	0.00	0.00	0.00	0.00	0.00	21.93	26.72	24.92	23.20	136.26	
		Catchment Area* (m ²) = 2554.00	Monthly Volumes													
		Catchment 305(Developme nt)	Precipitation (mm)	58.80	70.10	81.60	80.20	83.50	89.20	88.40	69.10	87.20	66.80	62.30	58.00	895.20
			Evaporation Factor	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	-
			Run-Off Coefficient	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	-
			Evaporation (mm)	8.82	10.52	12.24	12.03	12.53	13.38	13.26	10.37	13.08	10.02	9.35	8.70	134.28
	Run-Off (mm)		49.98	59.59	69.36	68.17	70.98	75.82	75.14	58.74	74.12	56.78	52.96	49.30	760.92	
	Catchment Area (m ²) = 9852.00	Monthly Volumes														
	Total AET (m ³)		0.00	85.39	200.09	284.06	280.63	240.56	201.64	98.70	25.25	0.00	0.00	0.00	1416.32	
	Total Evaporation (m ³)		86.89	103.59	120.59	118.52	123.40	131.82	130.64	102.12	128.86	98.72	92.07	85.71	1322.93	
	Total Infiltration (m ³)		90.11	56.18	4.99	0.00	0.00	0.00	0.00	0.00	84.02	102.36	95.47	88.88	522.01	
	Total Runoff (m ³)		552.47	624.49	686.66	671.61	699.25	746.98	740.28	578.66	786.24	627.64	585.36	544.96	7844.59	
	Site Total Monthly Volumes															
	Total AET (m ³)		0.00	223.52	523.72	743.52	734.54	629.67	527.78	258.34	66.08	0.00	0.00	0.00	3707	
	Total Evaporation (m ³)		176.96	210.96	245.57	241.36	251.29	268.44	266.04	207.95	262.42	201.03	187.49	174.55	2694	
	Total Infiltration (m ³)		235.85	147.06	13.07	0.00	0.00	0.00	0.00	0.00	219.91	267.93	249.89	232.64	1366	
	Total Runoff (m ³)		1159.98	1293.50	1400.28	1367.69	1423.97	1521.18	1507.53	1178.40	1633.68	1317.80	1229.03	1144.20	16177	



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