REPORT



27 WINONA DRIVE

WHITCHURCH-STOUFFVILLE, ONTARIO

NOISE IMPACT STUDY

RWDI #2406483 August 19, 2024

SUBMITTED TO

Darul Khair Center Stouffville

86 Ringwood Drive, Unit 36 Whitchurch-Stouffville, ON info@darulkhair.ca

Worship-Mosque

27 Winona Drive Whitchurch-Stouffville, ON L4A 2S9

SUBMITTED BY

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NOISE IMPACT STUDY 27 WINONA DRIVE

RWDI#2406483 August 19, 2024



VERSION HISTORY

Index	Date	Description	Prepared by	Reviewed by
1	June 13, 2023	Submitted for ZBA	Caelan Weber-Martin	Jacquie Kelton

NOISE IMPACT STUDY 27 WINONA DRIVE

RWDI#2406483 August 19, 2024



EXECUTIVE SUMMARY

RWDI was retained to prepare a Noise Impact Study for the proposed mosque, located at 27 Winona Drive in Whitchurch-Stouffville, Ontario. This assessment was completed to support the Zoning Bylaw Amendment (ZBA) submission as required by the Town of Whitchurch-Stouffville.

A screening level assessment of stationary sources associated with the mosque was conducted for existing and proposed surrounding buildings.

At this stage in design, the locations of the rooftop equipment have not been decided. HVAC units should be located as far towards the southwest corner of the mosque rooftop as feasible to minimize sound levels at surrounding noise-sensitive buildings.

The land immediately to the east of the proposed mosque, 28 Fairview Avenue, has an active development application. However, the development has yet not been approved. Since the land is currently zoned as Commercial Residential Mixed, allowing noise-sensitive uses for buildings with a maximum height of 20m, the proposed 28 Fairview Avenue development was conservatively included in this assessment to represent a potential future noise-sensitive building. Depending on the rooftop locations of the HVAC units and on the building orientation of a future noise-sensitive building at 28 Fairview Avenue, sound levels may exceed provincial guidelines. However, if this scenario occurs, various mitigation measures are considered feasible, including at-source mitigation measures such as barrier walls, and at-receptor mitigation measures such as including air conditioning in the building design which allows residents to keep windows closed and reduces indoor sound levels.

This assessment should be refined to include the correct rooftop locations of the HVAC equipment once the information is available. Based on the results of the analysis, the proposed mosque is feasible with respect to noise.



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1 INTRODUCTION

RWDI was retained to prepare a Noise Impact Study for the proposed mosque located at 27 Winona Drive in Whitchurch-Stouffville, Ontario. The context site plan is shown in **Figure 1**.

This assessment was completed in support of the Zoning Bylaw Amendment (ZBA) submission as required by the Town of Whitchurch-Stouffville. This assessment was based on design drawings dated June 13, 2023. A copy of the drawings is included in **Appendix A**.

2 APPLICABLE CRITERIA

Applicable criteria for stationary noise sources are adopted from the Ontario Ministry of the Environment, Conservation and Parks (MECP) NPC-300 Environmental Noise Guideline (MOE, 2013).

Noise from stationary sources requires sound levels to be assessed for the predictable worst-case one-hour average sound level (Leq) for each period of the day. For assessing sound originating from stationary sources, NPC-300 defines sound level criteria for two types of Points of Reception (PORs): outdoor and plane of the window.

The assessment criteria for all PORs is the higher of either the exclusion limit per NPC-300 or the minimum background sound level that occurs or is likely to occur at a POR. The applicable exclusion limit is determined based on the level of urbanization or "Class" of the area. The proposed development site would be characterized as a "Class 1 Area", which is defined according to NPC-300 as an area with an acoustical environment typical of a major population centre, where the background sound level is dominated by the activities of people, usually road traffic, often referred to as "urban hum."

The NPC-300 exclusion limits for continuously operating stationary sources in a Class 1 Area are summarized in **Table 1**.

Table 1: NPC-300 Exclusion Limits for Continuous Sources

Time Period	Class 1 Area		
Time Period	Outdoor	Plane of Window	
Daytime 07:00-19:00	50 dBA	50 dBA	
Evening 19:00-23:00	50 dBA	50 dBA	
Nighttime 23:00-07:00		45 dBA	



3 STATIONARY SOURCE ASSESSMENT

3.1.1 Surrounding Noise-Sensitive Receptors

Lands surrounding the proposed mosque consist of:

- Stouffville Auto Wash Car Wash to the north with residential dwellings beyond that,
- A property with development applications pending to the east (28 Fairview Avenue),
- A commercial plaza to the immediate south,
- Future residential developments to the south (along the south side of Main Street), and
- A commercial plaza to the west.

Representative worst-case receptors were selected to represent the dwellings to the north. A façade receptor with a height of 4.5m was used to represent the worst-case façade sound level at the 2nd storey (or 1.5m receptor height for single-storey dwellings). An outdoor receptor with a height of 1.5m was used to assess sound levels in the backyards of the dwellings.

The building shape of the proposed 28 Fairview Avenue was used to assess noise at the lot to the east, with a building height of 20 meters (maximum building height for the current zoning). A worst-case façade receptor was used to assess sound levels at the potential future building. The ZBA for the proposed 28 Fairview Avenue development has currently not been approved, however, the building was conservatively considered in this assessment to account for the case where the development is approved in the future, or if another noise-sensitive building is built on the lot. However, a future development should consider noise from the mosque in their own Noise Impact Study to ensure that appropriate sound levels are met at their building.

Future residential developments to the south, along the south side of Main Street, were included in this assessment. Sound levels were assessed at worst-case façade locations for future developments.

Representative receptor locations included in this assessment are illustrated in Figure 2.

3.1.2 Stationary Source Modelling

Stationary sources associated with the proposed mosque include 3 rooftop HVAC units and one transformer. There will be no call-to-prayer sound system associated with the proposed mosque. Sound power level data was provided for the 3 HVAC units and is included in **Appendix B**. The transformer associated with the mosque is a small 300 kVA transformer and is considered insignificant from a noise perspective relative to the HVAC units. Therefore, this assessment does not include the transformer.

Since the locations of the rooftop equipment are not currently known, the HVAC units were assumed to be on the west side of the rooftop. The assumed locations of the units are shown in **Appendix C** in **Figure C.1**.

Sound power levels for the HVAC units are shown in **Table 2**.



Table 2: Stationary Source Sound Power Levels

	Source ID	Sound	Duty Cycle		
Source Description	(As shown in Figure C.1)	Power Level (dBA)	Daytime and Evening (07:00 – 23:00)	Nighttime (23:00h - 07:00)	
12.5 Ton HVAC Unit	JAIN_12_5_T	89	Continuous	30 minutes/hour	
15 Ton HVAC Unit	JAIN_15_T	87	Continuous	30 minutes/hour	
7.5 Ton HVAC Unit	JAIN_7_5_T	86	Continuous	30 minutes/hour	

The HVAC units were assumed to operate continuously during the daytime and evening, and 30 minutes per hour during nighttime. These assumptions can be refined, if necessary, once information is available regarding the unit locations, to include a more realistic representation of the nighttime operating scenario.

3.1.3 Analysis and Results

Stationary source noise modelling was carried out using the Cadna/A software package, a commercially available implementation of the ISO 9613 (ISO, 1994 and ISO, 1996) algorithms. The predicted sound levels are assessed against the Class 1 Area limits. A sample calculation is included in **Appendix C** for the worst-case façade receptor associated with the proposed 28 Fairview Avenue building (R04).

Table 3: Predicted Sound Levels at Worst-case Receptor Locations - Continuous Stationary Sources

		Predicted Sound	Criteria	Meets Class 1 Criteria?	
Receptor	Receptor Description	Level Daytime-Evening / Nighttime LEQ-1hr (dBA)	Class 1 Daytime-Evening / Nighttime L _{EQ-1hr} (dBA)		
R01_f	Façade Receptor – 1-Storey House at 50 Winona Drive	45 / 42	50 / 45	Yes / Yes	
R01_o Outdoor Receptor – 1-Storey House at 50 Winona Drive		47 /[1]	50 /[1]	Yes / ^[1]	
R02_f	Façade Receptor – 1-Storey House at 336 Rupert Avenue	38 / 35	50 / 45	Yes / Yes	
R02_o	Outdoor Receptor – 1-Storey House at 336 Rupert Avenue	37 /[1]	50 /[1]	Yes / ^[1]	
R03_f	Façade Receptor – 1-Storey House at 34 Fairview Avenue	34 / 31	50 / 45	Yes / Yes	



		Predicted Sound	Criteria	
Receptor	Receptor Description	Level Daytime-Evening / Nighttime L _{EQ-1hr} (dBA)	Class 1 Daytime-Evening / Nighttime Leq-1hr (dBA)	Meets Class 1 Criteria?
R03_o	Outdoor Receptor – 1-Storey House at 34 Fairview Avenue	32 / ^[1]	50 / ^[1] dBA	Yes / ^[1]
R04	Façade Receptor – Future Potential 28 Fairview Avenue Development	48 / 45	50 / 45 dBA	Yes / Yes
R05	Façade Receptor – Future 5991 Main Street Development	43 / 40	50 / 45 dBA	Yes / Yes
R06 Façade Receptor – Future 5945-5947 Main Street Development		43 / 40	50 / 45 dBA	Yes / Yes

Note(s):

- 1. Outdoor areas are not assessed during the nighttime period.
- 2. No outdoor points of reception were identified for R04, R05, or R06.

As shown in **Table 3**, based on the modelling assumptions, the continuous sound levels at the façade due to stationary sources are predicted to meet the applicable Class 1 sound level criteria for all surrounding noise-sensitive receptors.

Currently, the proposed development at 28 Fairview Avenue has not been approved for ZBA. Furthermore, the assumed HVAC unit locations at the mosque and the building orientation for the proposed 28 Fairview Avenue may not be realistic. This assessment should be re-visited once more information is known regarding the HVAC unit locations and the future 28 Fairview Avenue building orientation. If a future development is proposed at 28 Fairview Avenue after the approval of the proposed 27 Winona Drive mosque, the development should consider noise from the mosque in their Noise Impact Study.

Rooftop HVAC units for the proposed mosque should be located as far to the southwest as feasible to minimize sound levels at surrounding noise-sensitive lands. It is recommended that a design review be completed once the HVAC locations are confirmed to ensure the final design meets the required sound level criteria.



4 CONCLUSIONS

RWDI was retained to prepare a Noise Impact Study for the proposed mosque located in Whitchurch-Stouffville, Ontario.

A screening level assessment of stationary sources associated with the mosque was conducted for existing and proposed surrounding buildings. At this stage in design, the locations of the rooftop equipment have not been decided. HVAC units should be located as far towards the southwest corner of the mosque rooftop as feasible to minimize sound levels at surrounding noise-sensitive buildings. A detailed design review should be completed once the HVAC locations are confirmed to ensure the mosque meets the applicable sound level criteria at the surrounding sensitive receptors.

Based on the results of the analysis, the proposed mosque is feasible with respect to noise.

5 REFERENCES

- 1. Ontario Ministry of the Environment (MOE), August 2013, Publication NPC-300, Environmental Noise Guideline Stationary and Transportation Sources Approval and Planning (MOE, 2013).
- 2. International Organization for Standardization (ISO), 1994b, International Standard ISO 9613-1:1994, Acoustics Attenuation of Sound during propagation outdoors. Part 1: Calculation of the absorption of sound by the atmosphere. (ISO, 1994).
- 3. International Organization for Standardization (ISO), 1996, International Standard ISO 9613-2:1996, Acoustics Attenuation of sound during propagation outdoors Part 2: General method of calculation (ISO, 1996).



STATEMENT OF LIMITATIONS

This report entitled 27 Winona Drive was prepared by Rowan Williams Davies & Irwin Inc. ("RWDI") for Darul Khair Center Stouffville ("Client"). The findings and conclusions presented in this report have been prepared for the Client and are specific to the project described herein ("Project"). The conclusions and recommendations contained in this report are based on the information available to RWDI when this report was prepared. Because the contents of this report may not reflect the final design of the Project or subsequent changes made after the date of this report, RWDI recommends that it be retained by the Client during the final stages of the project to verify that the results and recommendations provided in this report have been correctly interpreted in the final design of the Project.

The conclusions and recommendations contained in this report have also been made for the specific purpose(s) set out herein. Should the Client or any other third party utilize the report and/or implement the conclusions and recommendations contained therein for any other purpose or project without the involvement of RWDI, the Client or such third party assumes any and all risk of any and all consequences arising from such use and RWDI accepts no responsibility for any liability, loss, or damage of any kind suffered by Client or any other third party arising therefrom.

Finally, it is imperative that the Client and/or any party relying on the conclusions and recommendations in this report carefully review the stated assumptions contained herein and to understand the different factors which may impact the conclusions and recommendations provided.



FIGURES

Site Context Plan

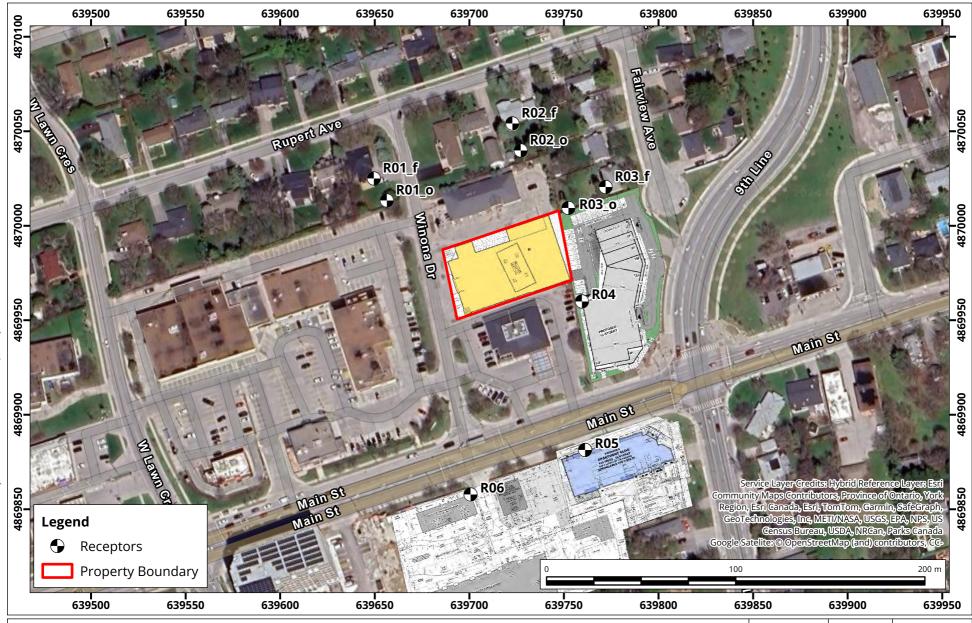
Map Projection: NAD 1983 UTM Zone 17N 27 Winona Drive - Witchurch-Stoufville, Ontario

True North Drawn by:CWM Figure:

Approx. Scale: 1:2,500

Date Revised: Aug 19, 2024 Project #: 2406483





Sensitive Receptor Locations

Project #: 2406483

True North Drawn by:CWM Figure:

Approx. Scale: 1:2,000

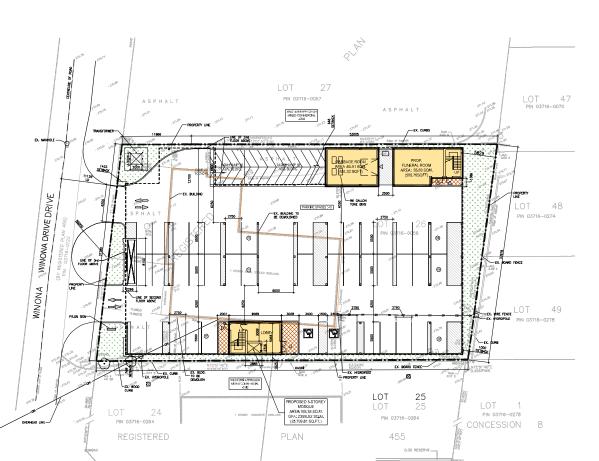
Date Revised: Aug 16, 2024

Map Projection: NAD 1983 UTM Zone 17N 27 Winona Drive - Witchurch-Stoufville, Ontario



APPENDIX A







5.18 m WIDENING MAIN STREET



SCALE: N.T.S.
PROJECT STATISTICS

ADDRESS: 27 , WINONA DR, WHITCHURCH, STOUFVILLE, ON		
	REQUIRED	PROPOSED
ZONING: COMMERCIAL RESIDENTIAL MIXED -WESTERN APPROACH(CM2) (BYLAW 2010-001-70 TOWN OF WHITCHURCH STOUFVILLE,2010)	CM-2	CM-2
LOT AREA (SQ.M)	O SQM. (MIN)	2419.62 SQ. (0.59 ACRES
LOT FRONTAGE		37.78 M
LOT DEPTH		64.99 M
BUILDING COVERAGE	N/A	183.90 SQ.M (7.60%)
GFA (SQ.M)		2388.52 SQ.
LANDSCAPED AREA	MIN.4.5N B/W STREET OF PARKING AREAS OR DRIVEWAYS	322.64 SQ.N (13.33%)
CONC. PAVED AREA		31.75 SQ.M. (1.38%)
MAX. BUILDING HEIGHT	20M	9.75M
PARKING	100	59
BUILDING SETBACKS	REQUIRED	PROPOSED
FRONT YARD (WEST)	(MIN)3 M (MAX)3 M	1.43 M
REAR YARD (EAST)	(MIN)D M	1.00 M
INTERIOR SIDE YARD (NORTH)	(MIN)0 M	0.64 M
INTERIOR SIDE YARD (SOUTH)	(MIN)O M	0.76 M
PARKING CALCULATION	REQUIRED	PROPOSED
PLACE OF WORSHIP: 10 PARKING SPACES FOR EACH 100 M ² OF GFA DEVOTED TO PUBLIC USE (585.99 SQM.)	58	
FITNESS AREA/BASKETBALL COURT (6 PARKING SPACE FOR EACH 100 M²) (458.53 SQ.M.)	27	60
OFFICE: 5 PARKING SPACES FOR EACH 100 M ² OF GFA (20.66 SQ.M.)	01	
FUNERAL ROOM 7.5 SPACES PER 100 M ² OF GFA (55.63 SQ.M.)	04	
CLASSROOMS 2 SPACES PER CLASSROOM	08	
TOTAL # PARKING SPACES	98	
DIFFERENCE	-38	
ACCESSIBLE PARKING: 26-100 PARKING SPACES = 1SPACE+4% OF TOTAL REQUIRED PARKING	04	04
LOADING CALCULATION:		
OVER 950M ² UP TO 2,400M ² OF GFA 4 LARGE LOADING SPACES REQUIRED (9M X 3.5M)	02	00

AREA DISTRIBUTION	
SPACES	AREA
MEN' PRAYER HALL	361.25 SQM.
WOMEN'S PRAYER HALL	224.74 SQM.
CLASSROOMS	124.10 SQM.
FUNERAL ROOM	55.63 SQM.

OWNER'S INFO:

LEGE	ND
	PROPERTY LINE
	NEW BUILDING
1000	EXISTING BUILDING
	LANDSCAPE
388888	CONC. PAVEMENT, 150MM RAISED
	ASPHALT
Δ	MAIN DOOR ENTRANCE
Δ	OVERHEAD DOOR

LEGAL DESCRIPTION: PART PLAN OF LOT 26 REGISTERED PLAN 455 TOWN OF WHITCHURCH STOUFFVILLE REGIONAL MUNICIPALITY OF YORK

PLICANT:	
ARCHITECTURE INC. 20 Leslie Street,	
ite-208	
chmond Hill, ON. L4B 3J9	
416.256.9741	
Info@narchitecture.com	
ww.narchitecture.com	

GROUND FLOOR LEVEL

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CHECKED BY: NM	SCALE: AS NOTE
PROJECT NO.:	DRAWING NO.:

22-71



n Architecture Inc

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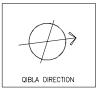
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PROJECT:

27 WINONA DR, WHITCHURCH STOUFFVILLE, ON PLACE OF WORSHIP-MOSQUE

SITE PLAN

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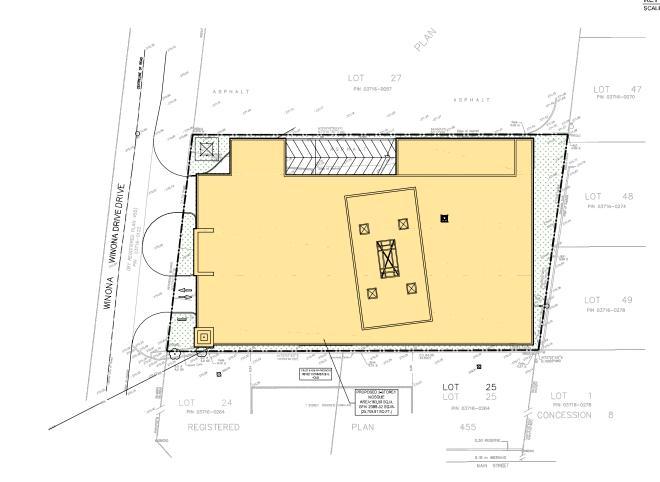
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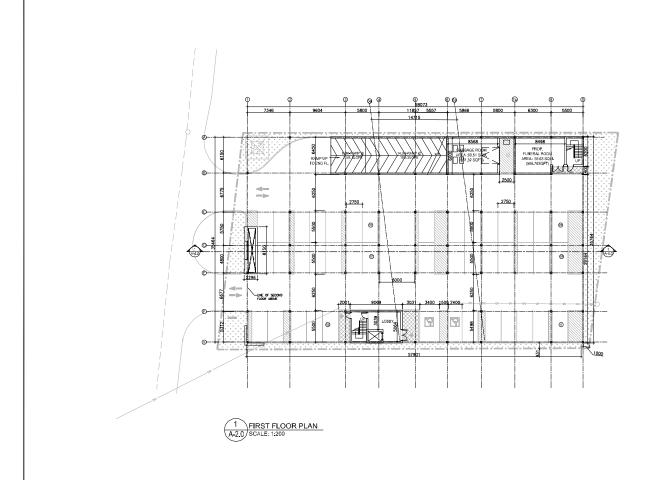
SITE PLAN SHOWING **ROOF PLAN**

1	
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1 SITE PLAN SHOWING ROOF PLAN A-1.0a SCALE: 1:150





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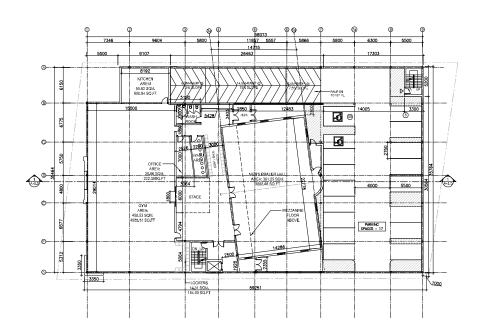
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FIRST FLOOR PLAN

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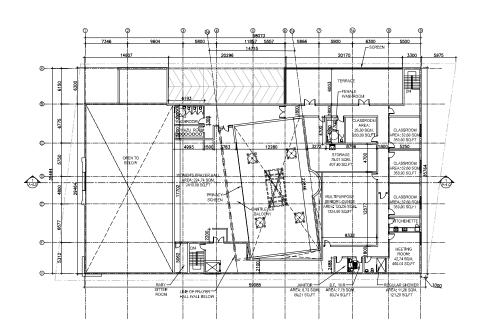
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2nd FLOOR PLAN

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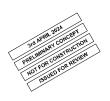


3rd FLOOR PLAN A-2.2 SCALE: 1:200



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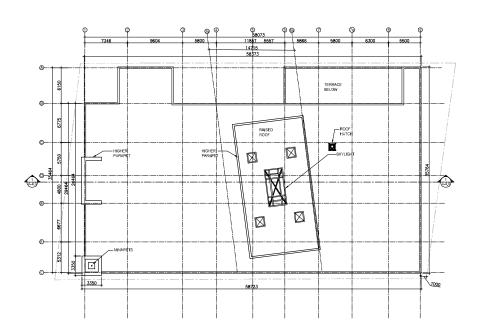
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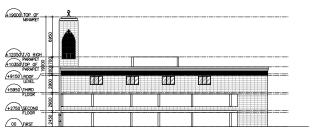
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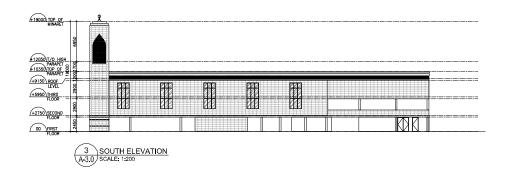
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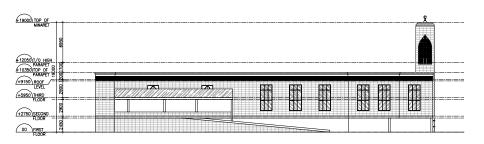
















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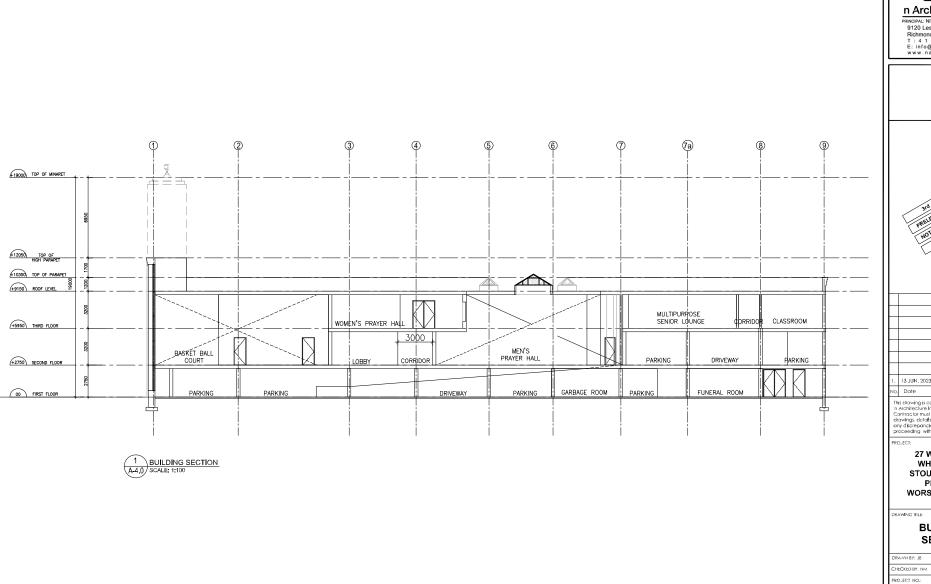
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BUILDING ELEVATION OPTION-4

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> BUILDING SECTION

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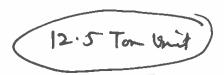
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APPENDIX B



Job Name: Moz Budget Pricing Prepared For: Unit Tag: JAIN = 12.5T Quantity: 1



Indoor Fan Data	Indoor Fan Performance
Airflow Application Downflow	Airflow 5000 cfm
Design ESP 1.000 in H2O	Supply Motor Horsepower, 4.600 hp
Component SP 0.432 in H2O	Indoor Motor Operating Power 2.864 hp
Heat SP 0.000 in H2O	Indoor RPM 1634 rpm
Total SP 1.432 in H2O	Outdoor Fan Data
Indoor Fan Drive Type Variable Direct	Outdoor Fan Drive Type Direct
Indoor Fan Quantity 1.00 Number	Outdoor Fan Quantity 1
Indoor Fan Type BC Plenum	Outdoor Fan Type Propeller
	Filters
	1st Filter Size and Qty 3 - 24 x 18 x 2
	2nd Filter Size and Qty 3 - 18 x 18 x 2

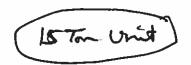
			Roof cu	rb 14" Full Peri	meter Knockdov	vn Curb		
North State of Lines, L	DRIV STALL	Economiza	er Conversion i	Kit None				A CONTRACTOR OF THE PARTY OF TH
	Symbio Ad	v Controls and	BACnet Conv	Kit None				
Acoustics								
Sound Path	63 Hz	125 Hz	250 Hz	500 Hz	1 kHz	2 kHz	4 kHz	8 kHz
Ducted Discharge	85 dB	90 dB	82 dB	74 dB	70 dB	67 dB	68 dB	67 dB
Ducted Inlet	82 dB	81 dB	76 dB	67 dB	64 dB	61 dB	61 dB	60 dB
Outdoor Noise	88 dB	91 dB	90 dB	87 dB	84 dB	80 dB	75 dB	67 dB

Note: Ducted Discharge/Ducted Inlet prediction data conform to AHRI 260

Warranty	
	Labor (first year) 1st Yr Labor Whole Unit



Job Name: Moz Budget Pricing Prepared For: Unit Tag; JAIN - 15T Quantity: 1



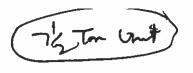
TO BE STORY			Roof cu	rb 14" Full Perir	meter Knockdov	vn Curb		
		Economiza	er Conversion i	Kit None	Versell and the			
	Symblo Ad	v Controls and	BACnet Conv I	Kit None		THURSDAY		
Acoustics				新版 國際			1000	
Sound Path	63 Hz	125 Hz	250 Hz	500 Hz	1 kHz	2 kHz	4 kHz	8 kHz
Ducted Discharge	79 dB	88 dB	77 dB	68 dB	63 dB	59 dB	59 dB	57 dB
Ducted Inlet	78 dB	84 dB	69 dB	63 dB	59 dB	56 dB	55 dB	53 dB
Outdoor Noise	84 dB	87 dB	88 dB	85 dB	82 dB	77 dB	74 dB	69 dB

Warranty		
	Labor (first year) 1st Yr Labor Whole Unit	14

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Job Name: Moz Budget Pricing Prepared For: Unit Tag: JAIN - 7.5T Quantity: 1



Indoor Fan Data	Indoor Fan Performance
Airflow Application Downflow	Airflow 3000 cfm
Design ESP 1.000 in H2O	Supply Motor Horsepower 3.000 hp
Component SP 0.151 in H2O	Indoor Motor Operating Power 1.281 hp
Heat SP 0.000 in H2O	Indoor RPM 1232 rpm
Total SP 1.151 in H2O	Outdoor Fan Data
door Fan Drive Type Variable Direct	Outdoor Fan Drive Type Direct
Indoor Fan Quantity 1.00 Number	Outdoor Fan Quantity 1
Indoor Fan Type BC Plenum	Outdoor Fan Type Propeller
	Filters
	1st Filter Size and Qty 2 - 18 x 24 x 2
	2nd Filter Size and Qty 3 - 24 x 16 x 2

		SELECT AND SERVICES	Roof cu	rb 14" Full Peri	meter Knockdov	vn Curb		
WIND BY BUILDING		Economize	er Conversion	Kit None				
	Symblo Ad	v Controls and	BACnet Conv	(It None				
Acoustics								
Sound Path	63 Hz	125 Hz	250 Hz	500 Hz	1 kHz	2 kHz	4 kHz	8 kHz
Ducted Discharge	79 dB	85 dB	77 dB	70 dB	65 dB	62 dB	62 dB	63 dB
Ducted injet	75 dB	74 dB	70 dB	58 dB	56 dB	53 dB	54 dB	54 dB
Outdoor Noise	84 dB	85 dB	84 dB	85 dB	82 dB	76 dB	73 dB	67 dB

	-35000	

Warranty

Labor (first year) 1st Yr Labor Whole Unit



APPENDIX C

Cadna/A ISO-9613 Calculation Protocol - Definitions

Parameter Unit Definition

Nr		Ray Number
х	(m)	X-axis Cartesian Coordinate
Υ	(m)	Y-axis Cartesian Coordinate
Z	(m)	Z-axis Cartesian Coordinate
Refl.	order	Order of Reflection
DEN	D/E/N	Time of Day (Day, Evening, or Night)
Freq.	(Hz)	1/1 Octave Band Dominant Frequency or Frequency Type ("A" for A-weighted)
Lw	(dBA)	Overall Sound Power Level
I/a	dB	Line/Area Source Correction
Optime	dB	Operating Time Correction
K0	(dB)	D_omega in ISO 9613-2 (correction for radiation into solid angles less than 4 Pi)
Di	(dB)	Directivity Index
Adiv	(dB)	Attenuation Due to Divergence
Aatm	(dB)	Atmospheric Attenuation
Agr	(dB)	Ground Attenuation
Afol	(dB)	Attenuation Due to Foliage
Ahous	(dB)	Attenuation from Houses
Abar	(dB)	Barrier Attenuation
Cmet	(dB)	Meteorological Correction
RL	(dB)	Reflection Loss
Lr	(dBA)	Resulting Noise Impact at Receptor - Leq (1-Hr)

Table C.1: Key Parameters Included in the Cadna/A Noise Modelling

27 Winona Drive

Parameter	Value	Rationale
Ground Absorption	0.2	Accounts for mostly hard ground (e.g., cement, pavement, packed dirt) surfaces between the proposed mosque and receptors of interest
Temperature	10 °C	Ontario standard conditions
Relative Humidity	70%	Ontario standard conditions
Max. Order of Reflection	2	Accounts for reflections from buildings



Stationary Source Locations

Project #: 2406483

True North Drawn by:CWM Figure: C.1

Approx. Scale: 1:2,000

Date Revised: Aug 19, 2024

Map Projection: NAD 1983 UTM Zone 17N 27 Winona Drive - Witchurch-Stoufville, Ontario Receiver

Name: 28 Fairview Avenue Potential Future Development - Worst-case Facade Receptor (10.5m Height)

ID: R04

X: 639759.55 m Y: 4869959.91 m Z: 10.50 m

	Point Source, ISO 9613, Name: "15 Ton Unit", ID: ""																			
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	dB(A)						
14	639710.69	4869974.97	10.65	0	D	Α	87.1	0.0	0.0	0.0	0.0	45.2	0.3	-2.4	0.0	0.0	0.0	0.0	0.0	44.0
28	639710.69	4869974.97	10.65	1	D	Α	87.1	0.0	0.0	0.0	0.0	56.3	0.8	-2.4	0.0	0.0	0.0	0.0	2.0	30.3

	Point Source, ISO 9613, Name: "12.5 Ton Unit", ID: ""																			
Nr.	Х	Υ	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	dB(A)						
34	639694.28	4869978.89	10.65	0	D	Α	89.2	0.0	0.0	0.0	0.0	47.6	0.3	-2.4	0.0	0.0	0.0	0.0	0.0	43.7
36	639694.28	4869978.89	10.65	1	D	Α	89.2	0.0	0.0	0.0	0.0	56.9	0.8	-2.4	0.0	0.0	0.0	0.0	2.0	31.9

	Point Source, ISO 9613, Name: "7.5 Ton Unit", ID: ""																			
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	dB(A)						
52	639699.96	4869959.85	10.65	0	D	Α	86.4	0.0	0.0	0.0	0.0	46.5	0.3	-2.4	0.0	0.0	0.0	0.0	0.0	42.0
57	639699.96	4869959.85	10.65	1	D	Α	86.4	0.0	0.0	0.0	0.0	56.0	0.8	-2.4	0.0	0.0	0.0	0.0	2.0	29.9
62	639699.96	4869959.85	10.65	2	D	Α	86.4	0.0	0.0	0.0	0.0	56.1	0.8	-2.4	0.0	0.0	0.0	0.0	13.3	18.5